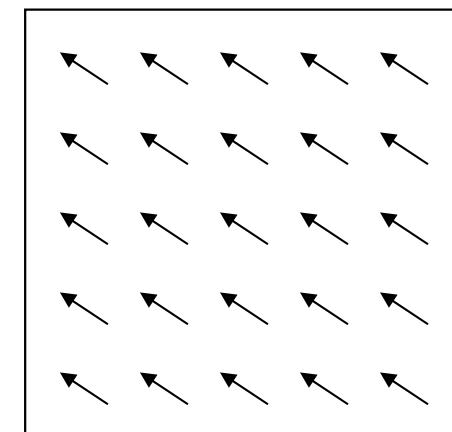
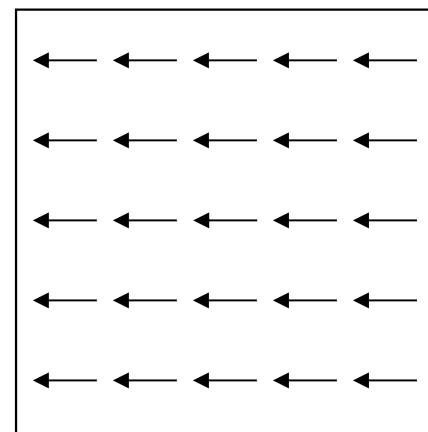
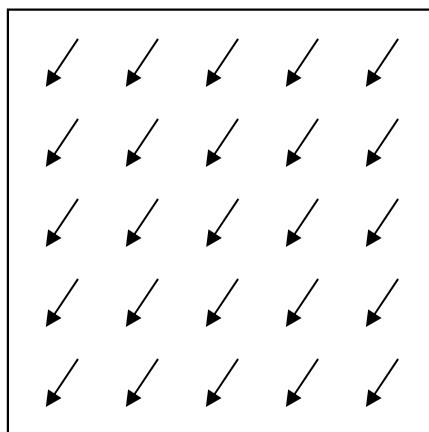
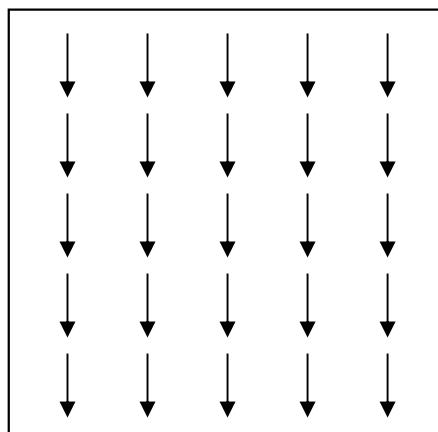
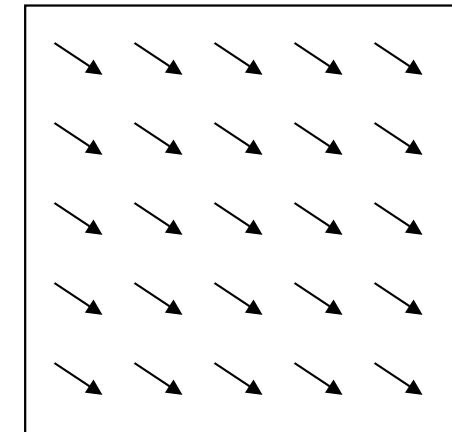
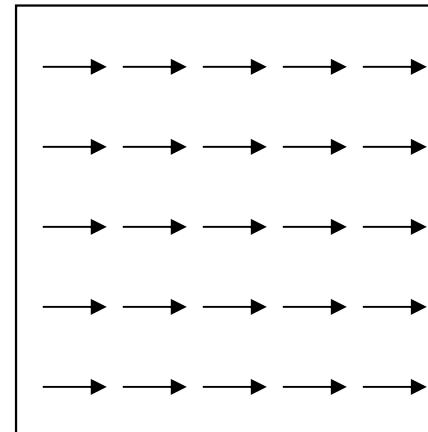
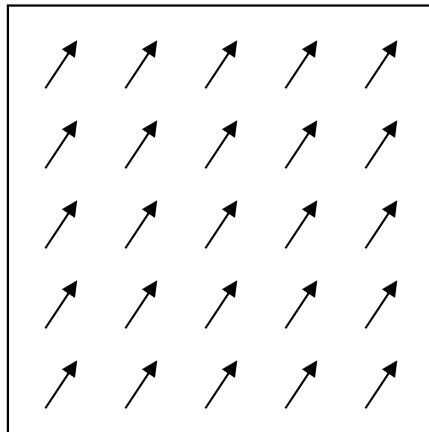
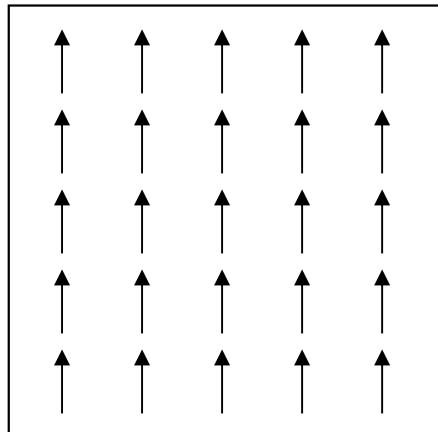


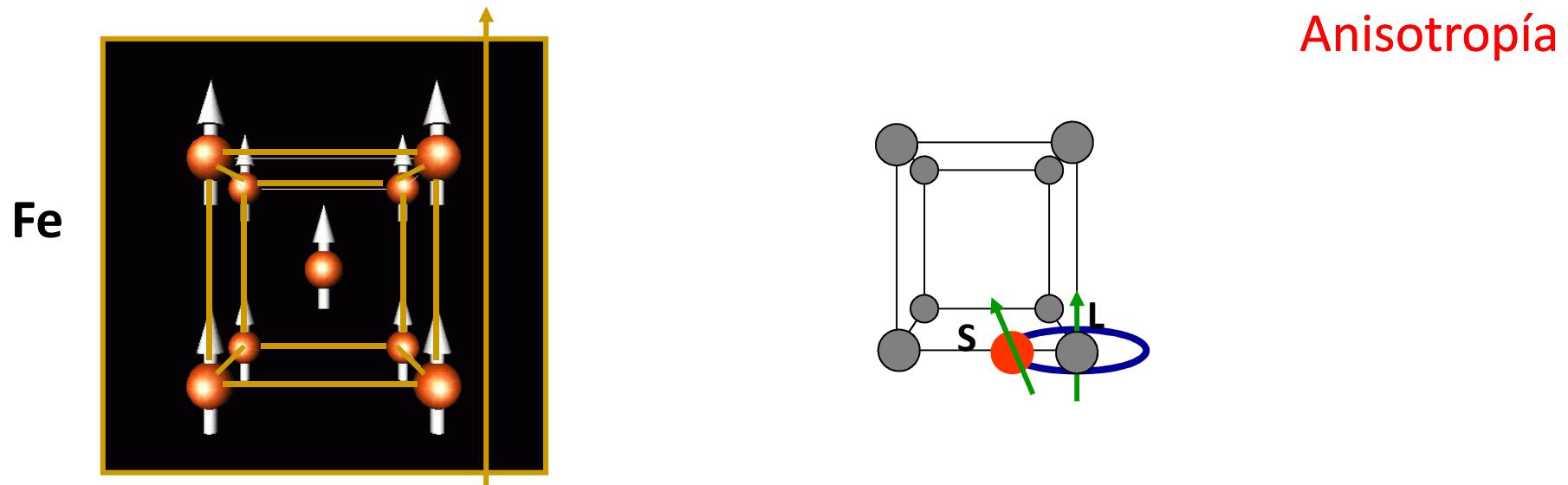
Anisotropía magnetocrystalina

Sólo intercambio
(ausencia de anisotropía)

Dirección aleatoria de \mathbf{M} en $4\pi \Rightarrow$ estado continuamente degenerado



Siempre estaríamos en presencia de un superparamagneto



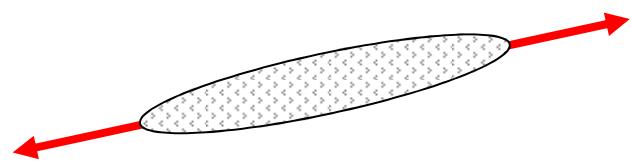
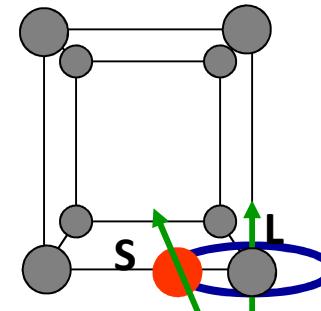
Estructura cristalina



Int. elect - Campo cristalino

+ interacción Spin – órbita

= Anisotropía magneto-cristalina

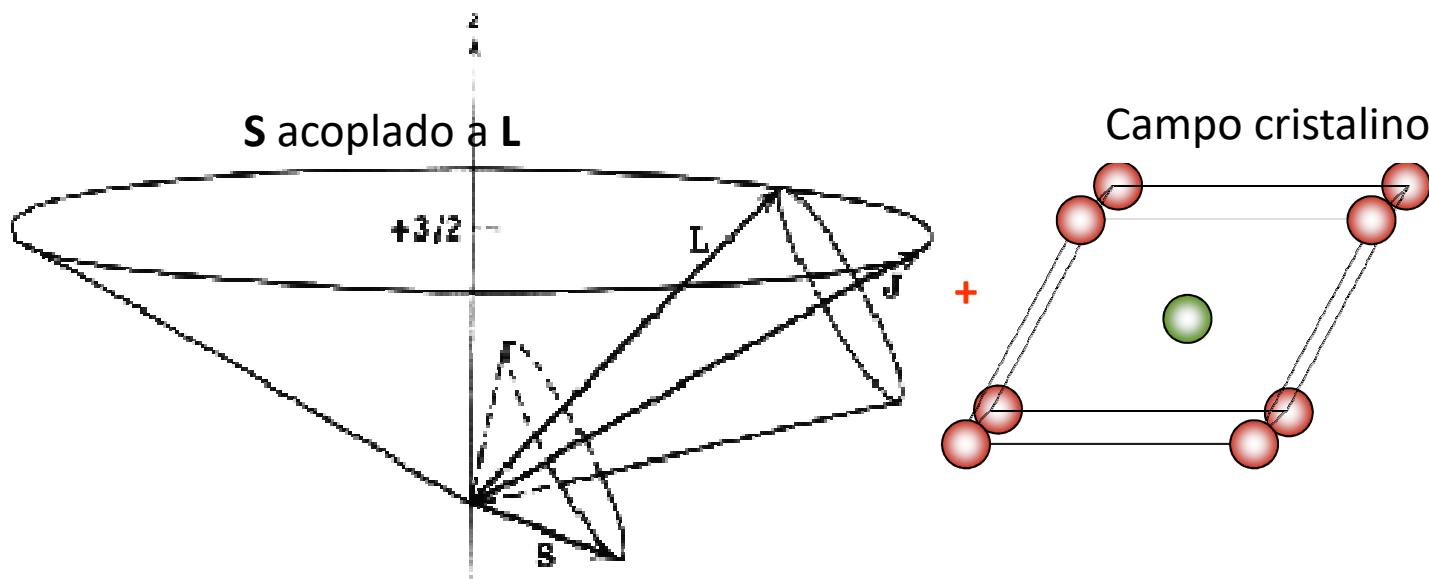


Forma: anisotropía magnetostática

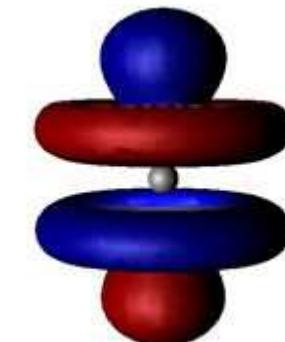
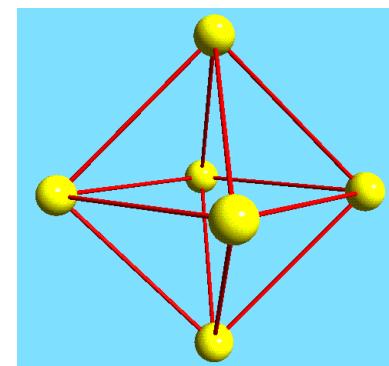
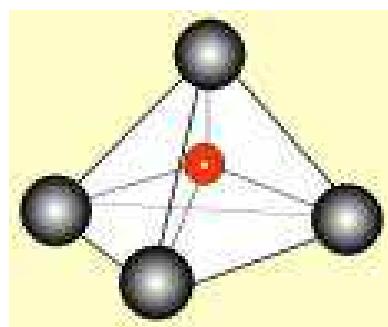


Esfuerzo: anisotropía magnetoelástica

spin – órbita + campo cristalino

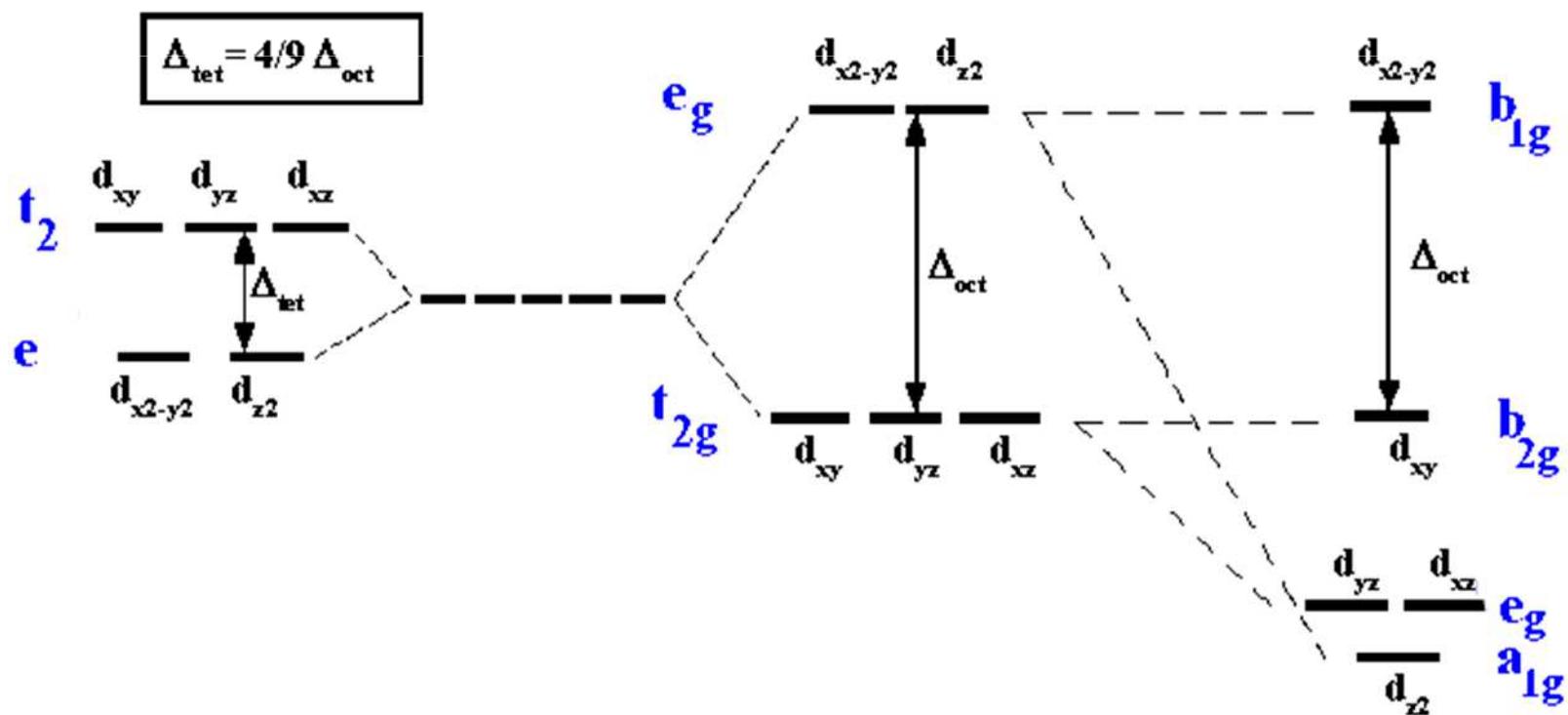
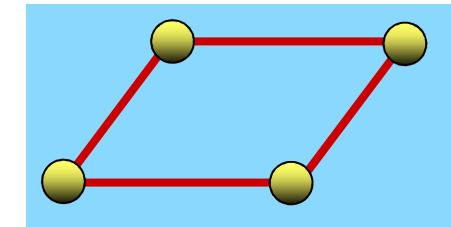
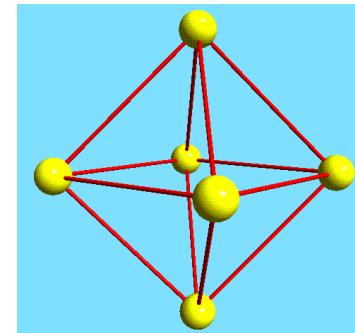
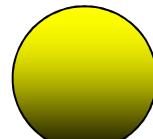
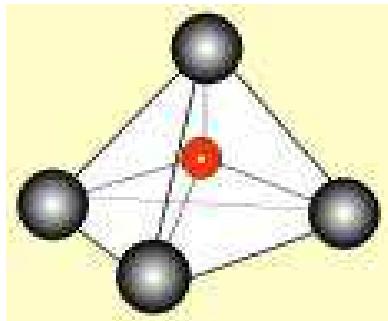


= $\begin{cases} \text{anisotropía} \\ \text{sobre} \\ \vec{L}, \vec{S} \text{ y } \vec{J} \end{cases}$



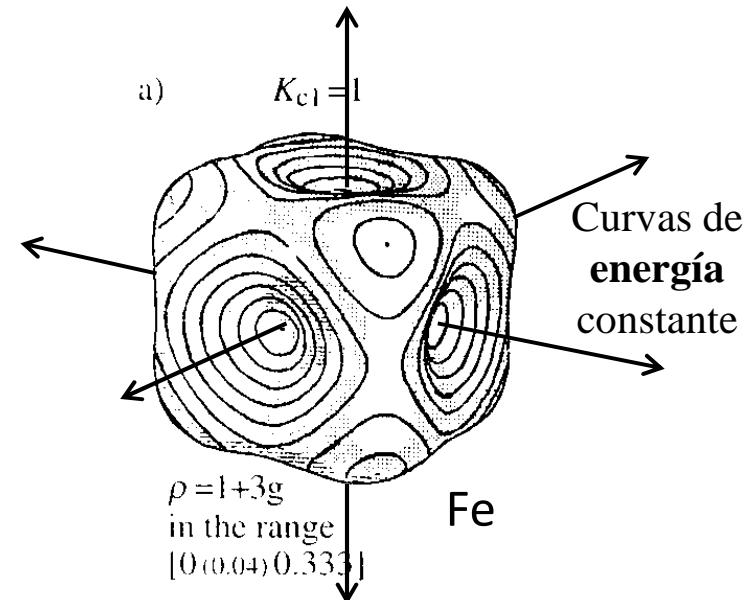
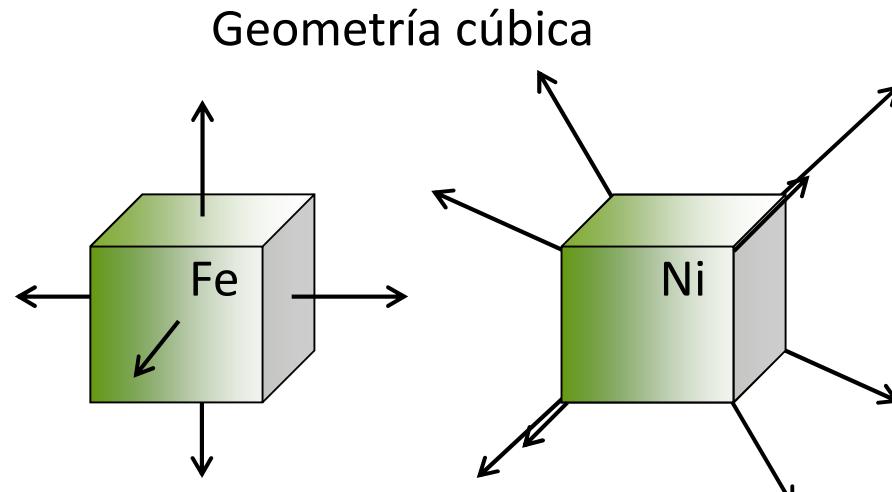
Diagramas de desdoblamiento de orbitales d por el campo cristalino

Campo tetraédrico ión libre campo octaédrico campo planar cuadrado

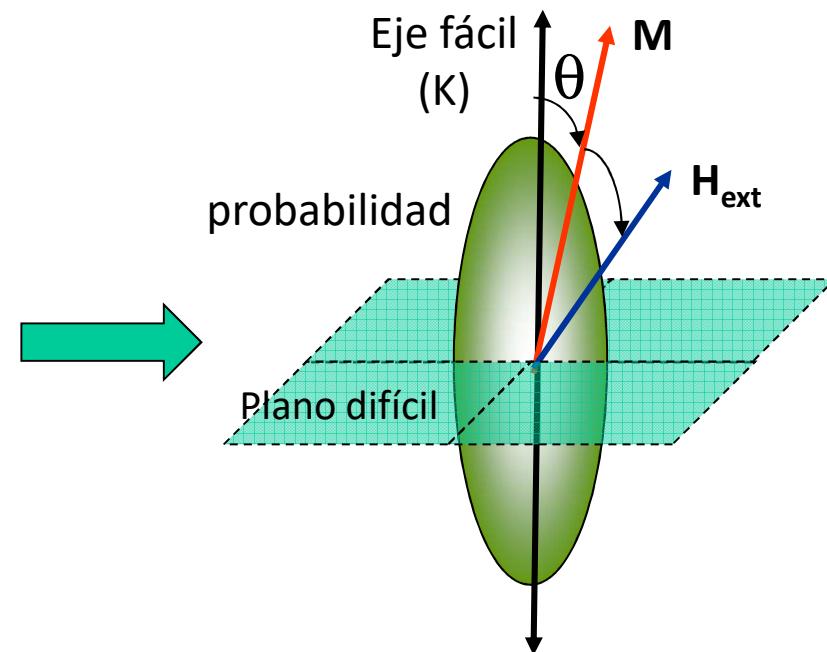
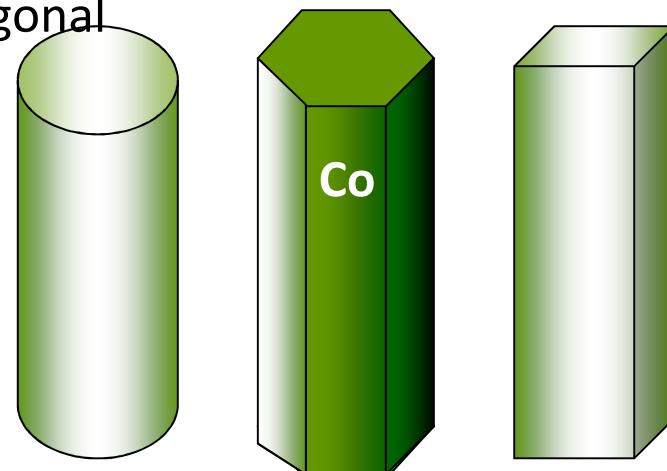


Energía de anisotropía Magnetocristalina

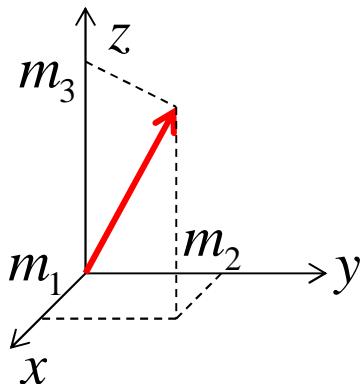
Definiciones



Geometría cilíndrica, tetragonal, hexagonal



Anisotropía – descripción fenomenológica



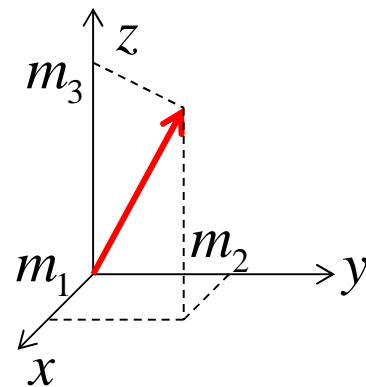
m_i cosenos directores de la magnetización

$$m_{1,2,3} = \frac{M_{x,y,z}}{M} \dots = \cos(\theta_{1,2,3})$$

e_K energía de anisotropía por unidad de volumen

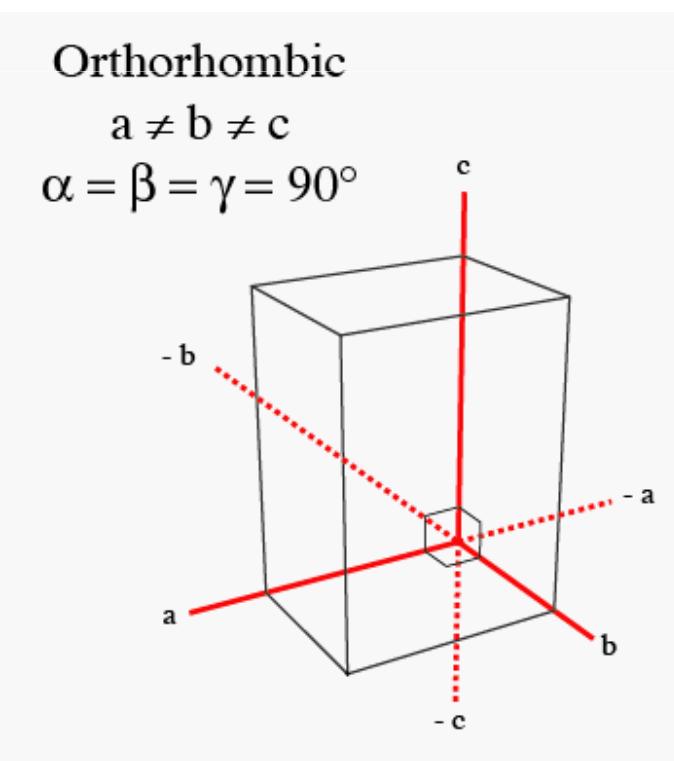
$$e_K = \sum_i K_i m_i^2 + \sum_{ij} K_{ij} m_i^2 m_j^2 + K_{123} m_1^2 m_2^2 m_3^2 + \sum_{ij} K'_{ij} m_i^4 m_j^4 + \dots$$

$$E_K \text{ energía de anisotropía} \quad E_K = \int e_K dV$$

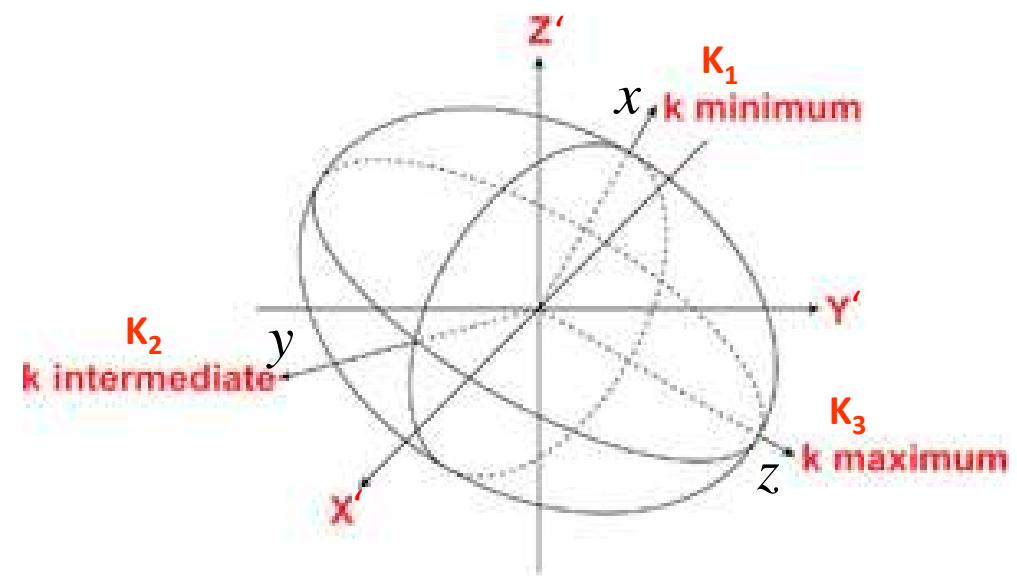


$$e_K = \sum_i K_i m_i^2 + \sum_{ij} K_{ij} m_i^2 m_j^2 + K_{123} m_1^2 m_2^2 m_3^2 + \sum_{ij} K'_{ij} m_i^4 m_j^4 + \dots$$

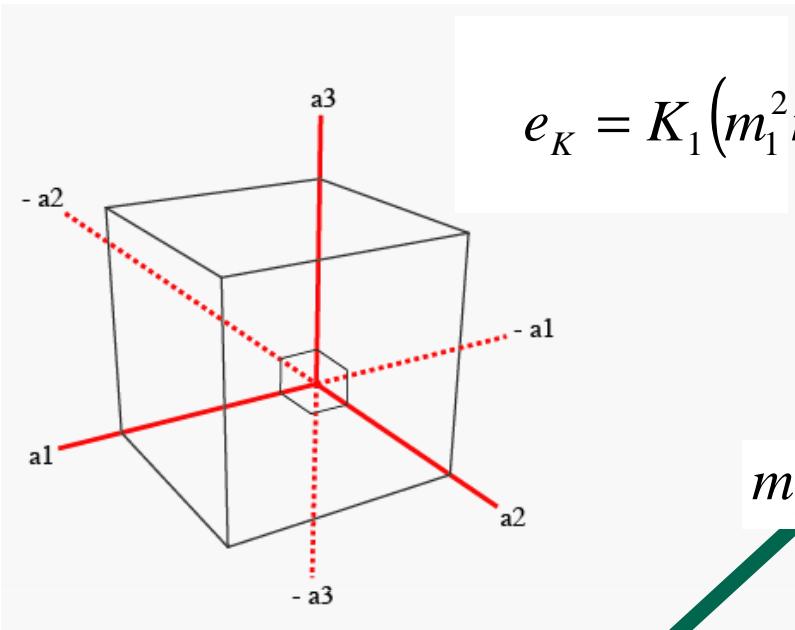
Ejemplo: sistema ortorrómbico



$$e_K \approx K_1 m_1^2 + K_2 m_2^2 + K_3 m_3^2$$



sistema cúbico



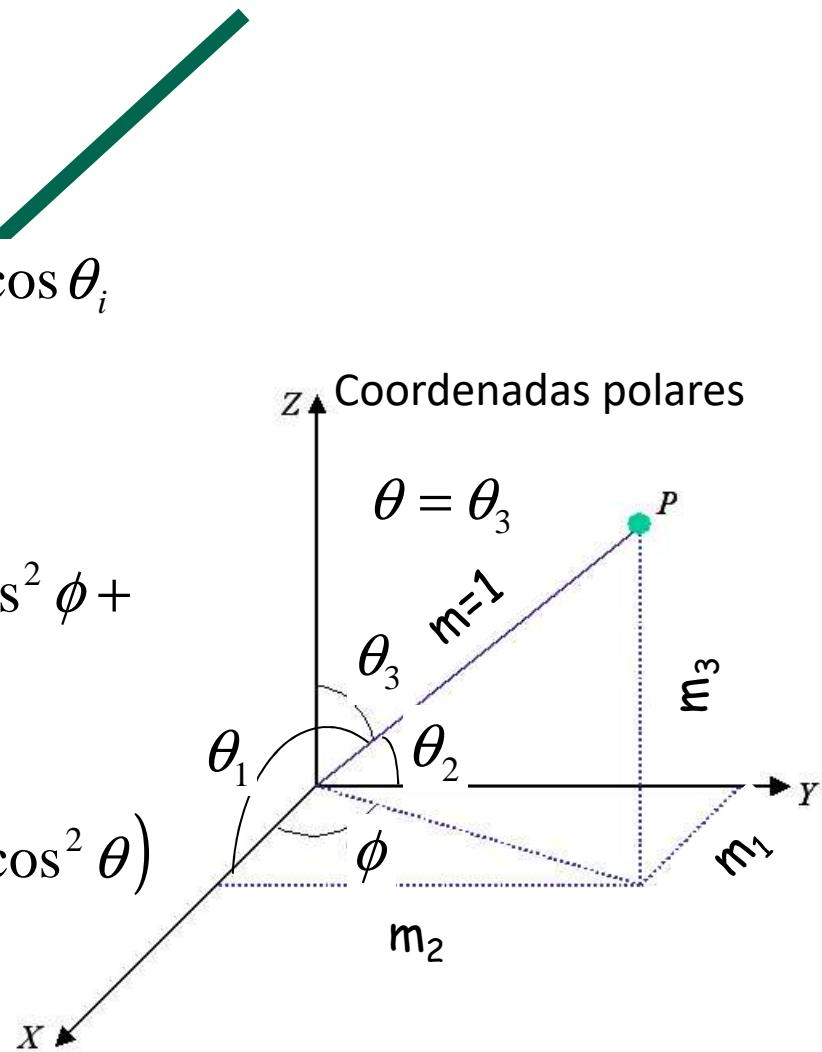
$$e_K = K_1(m_1^2 m_2^2 + m_1^2 m_3^2 + m_2^2 m_3^2) + K_2 m_1^2 m_2^2 m_3^2$$

$$m_i = \cos \theta_i$$

$$e_K = (K_1 + K_2 \cos^2 \theta) \sin^4 \theta \sin^2 \phi \cos^2 \phi + \\ + K_1 \sin^2 \theta \cos^2 \theta$$

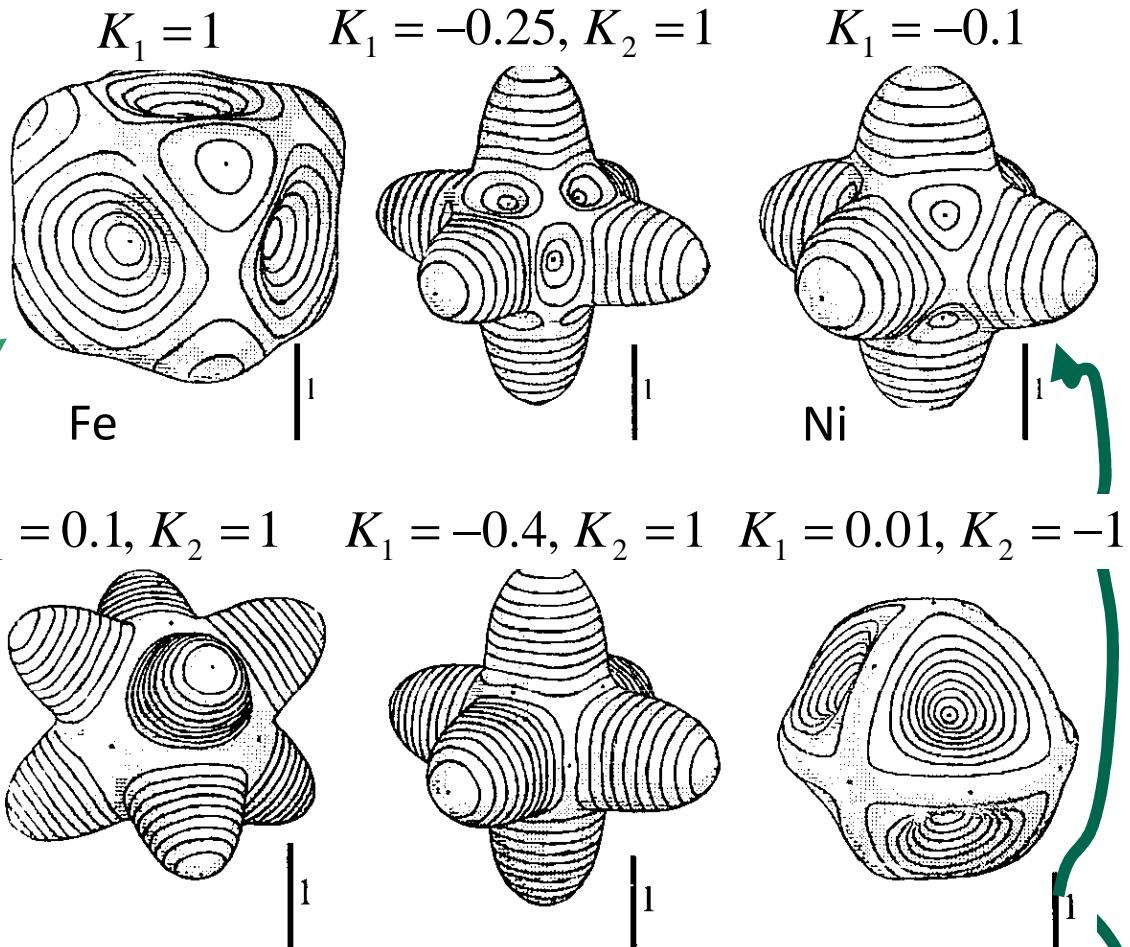
$$e_{K_1} = K_1 \sin^2 \theta (\sin^2 \theta \sin^2 \phi \cos^2 \phi + \cos^2 \theta)$$

$$e_{K_2} = K_2 \cos^2 \theta \sin^4 \theta \sin^2 \phi \cos^2 \phi$$



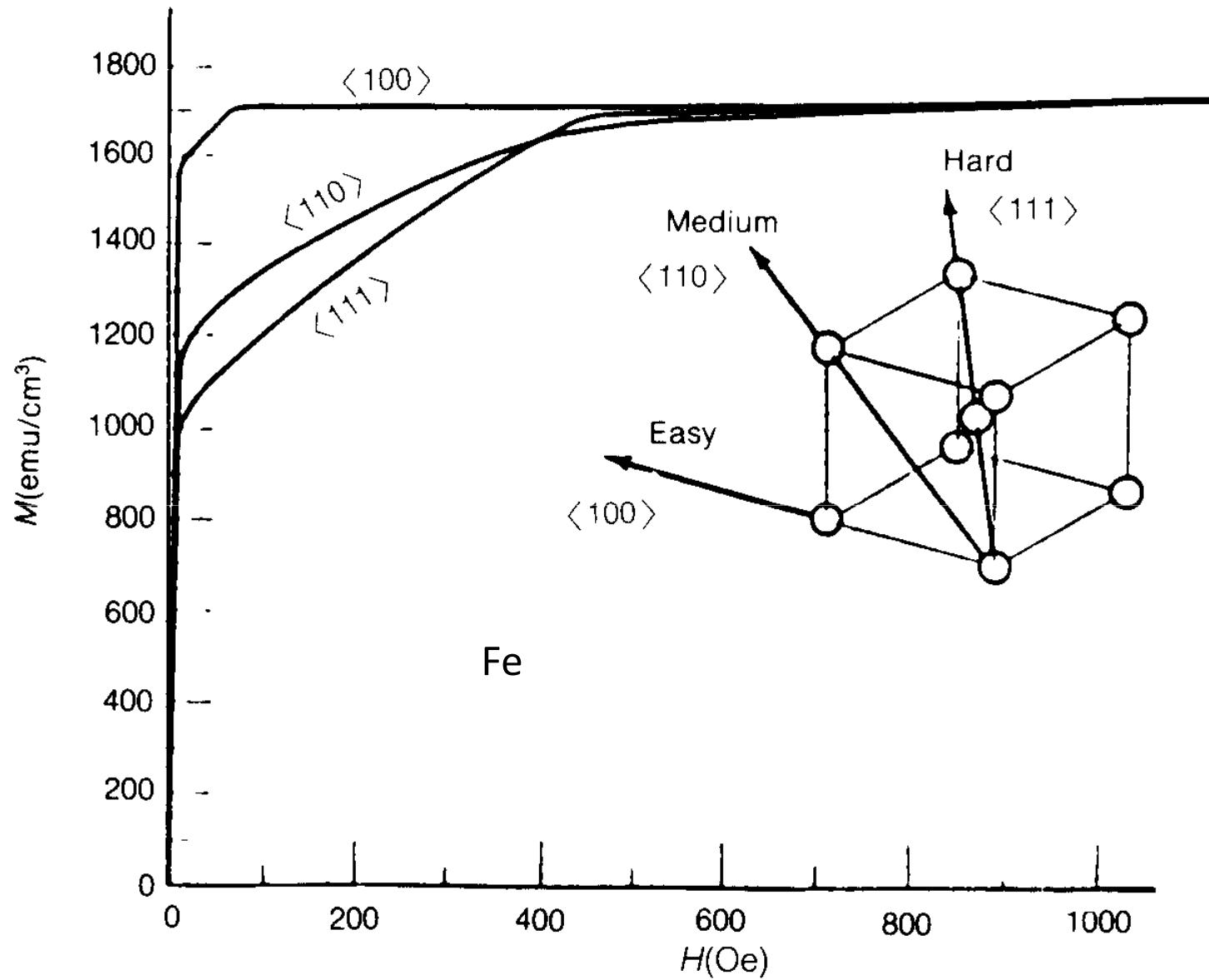
sistema cúbico
Curvas de energía constante

$$e_K = K_1(m_1^2 m_2^2 + m_1^2 m_3^2 + m_2^2 m_3^2) + K_2 m_1^2 m_2^2 m_3^2$$

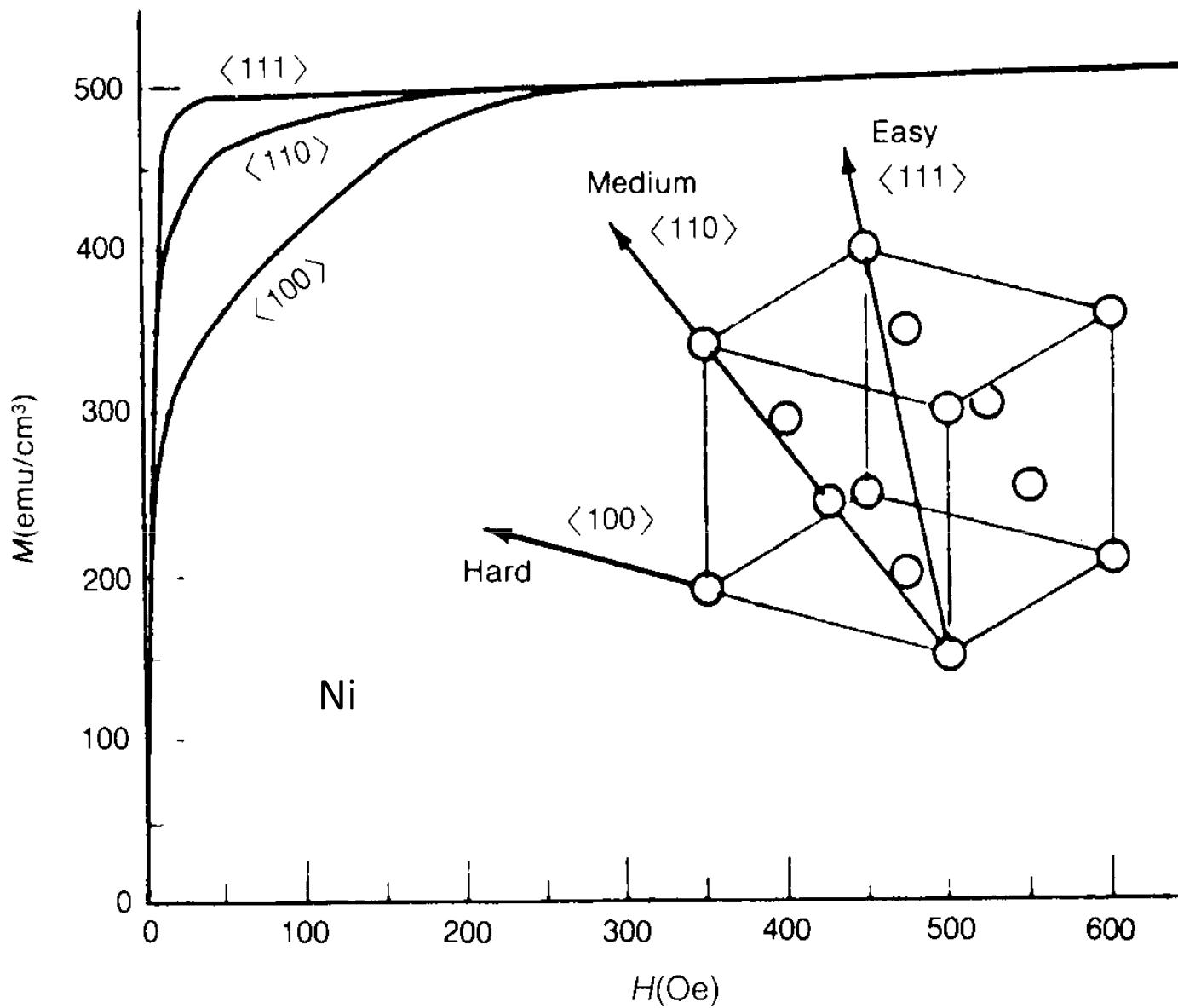


Material	K_1 (10^5 J/m^3)	K_2 (10^5 J/m^3)	Eje fácil
Fe	0.480	0.05	(100)
Ni	-0.045	-0.023	(111)

sistema cúbico

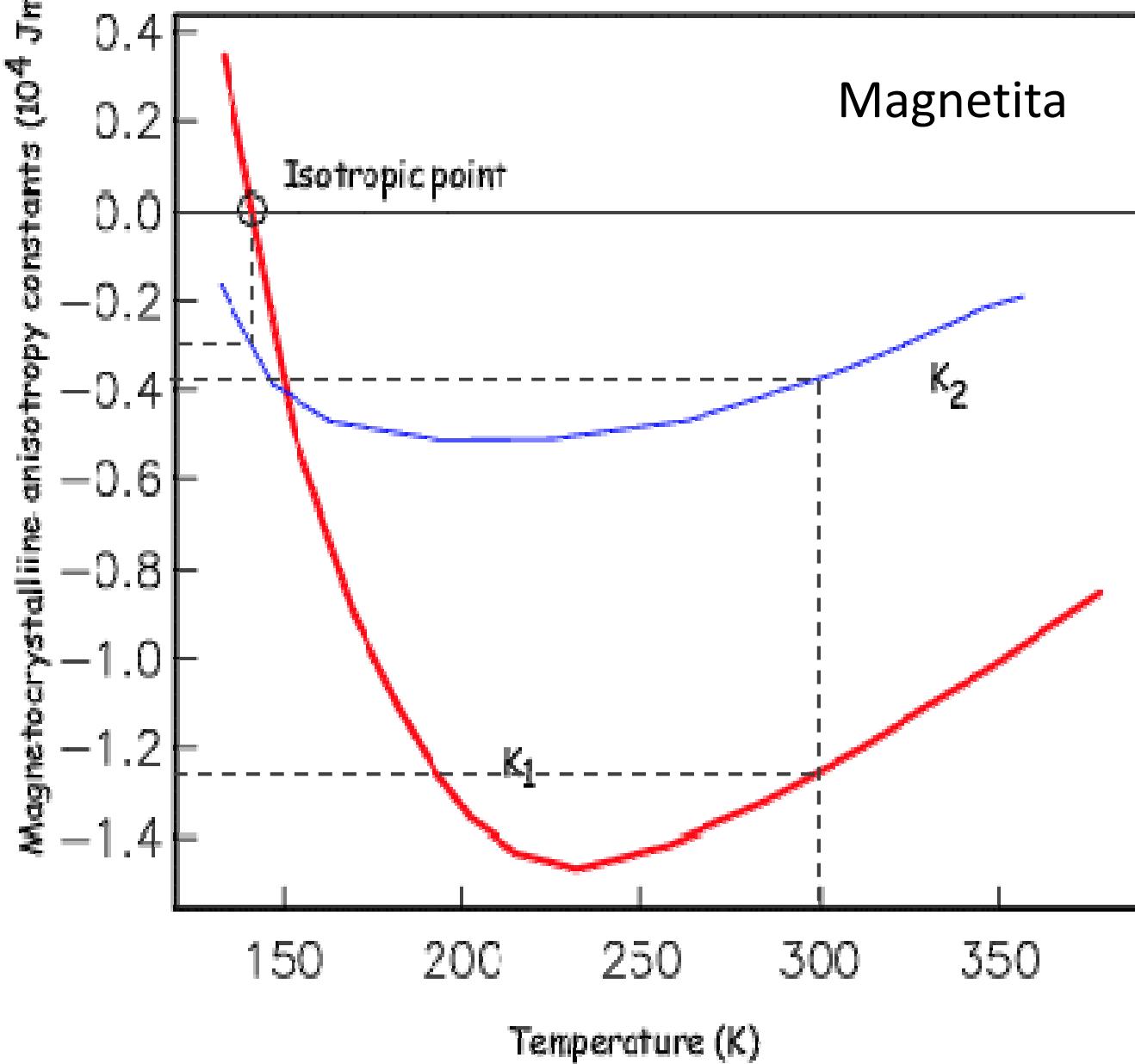


sistema cúbico

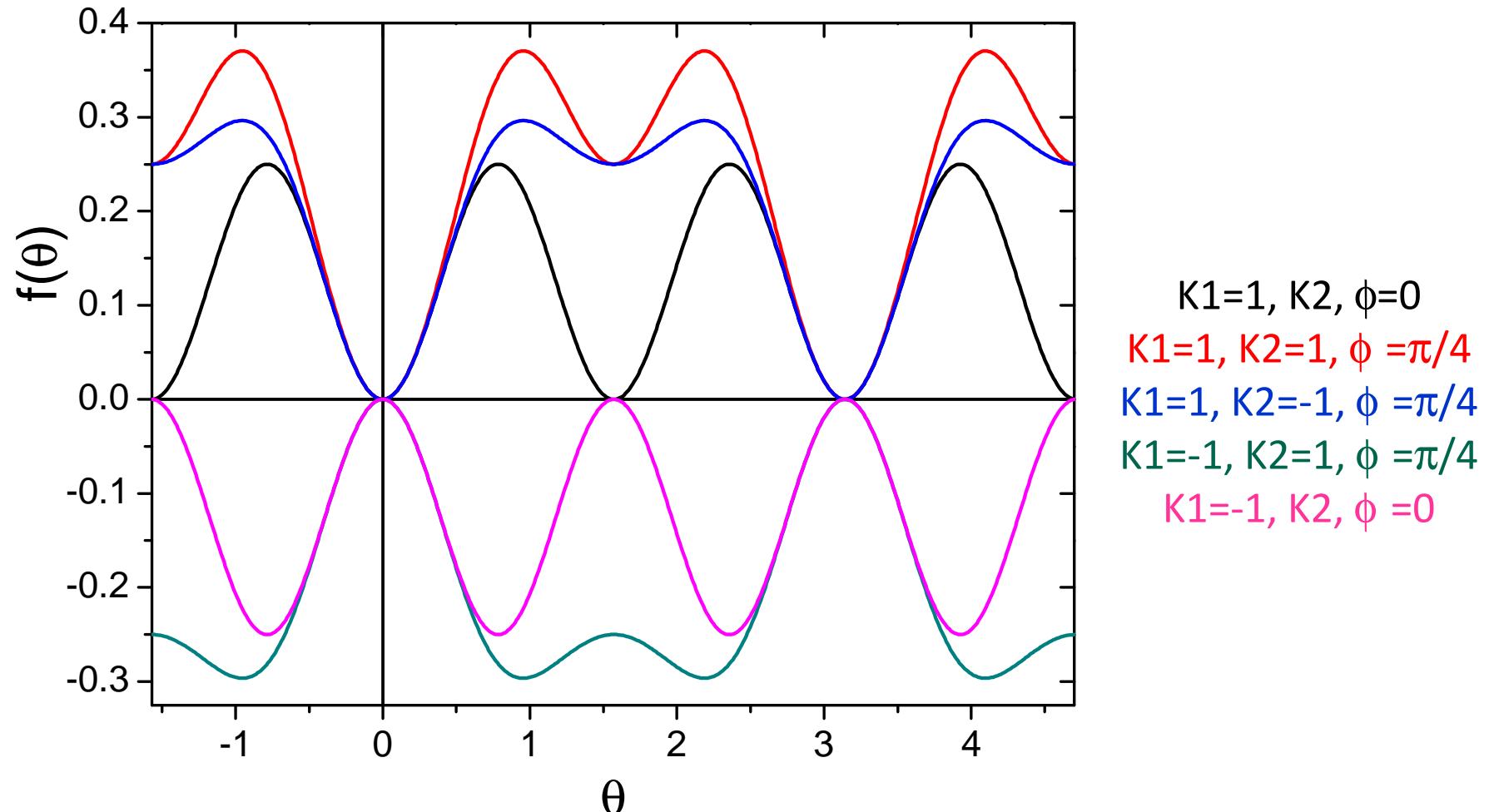


sistema cúbico

$$e_K = (K_1 + K_2 \cos^2 \theta) \sin^4 \theta \sin^2 \phi \cos^2 \phi + K_1 \sin^2 \theta \cos^2 \theta$$

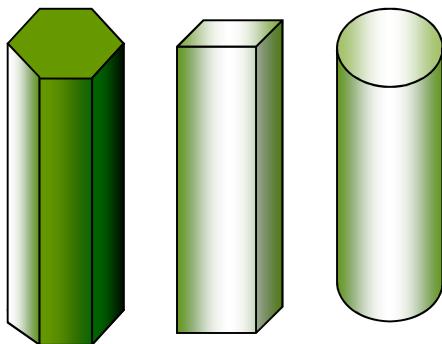
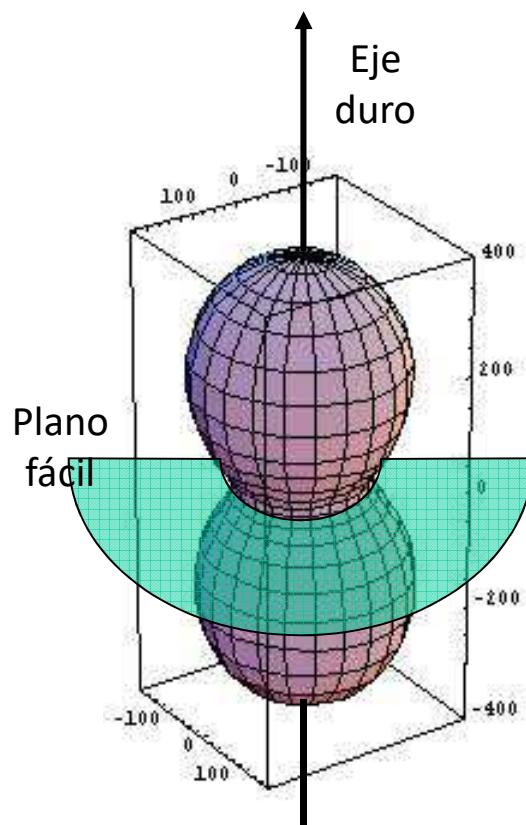


sistema cúbico

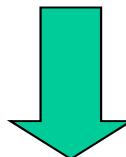


$$e_K = (K_1 + K_2 \cos^2 \theta) \sin^4 \theta \sin^2 \phi \cos^2 \phi + K_1 \sin^2 \theta \cos^2 \theta$$

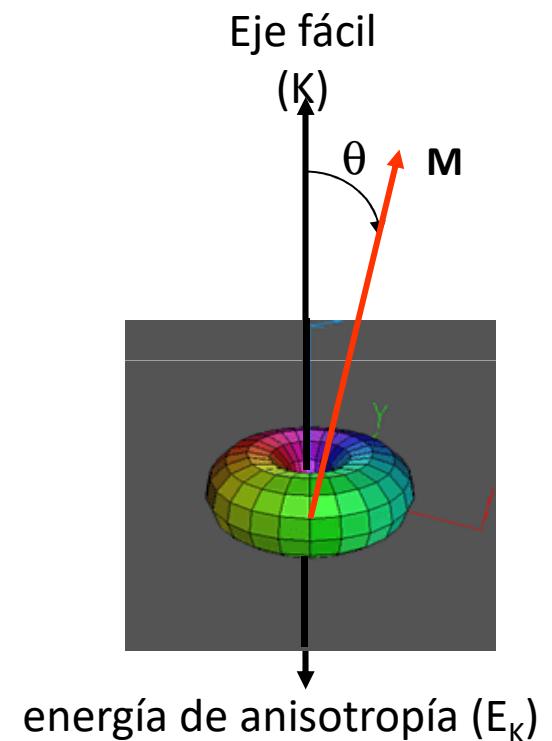
Sistemas hexagonal y tetragonal



$$e_K = K_1 \cos^2 \theta + K_2 \cos^4 \theta$$

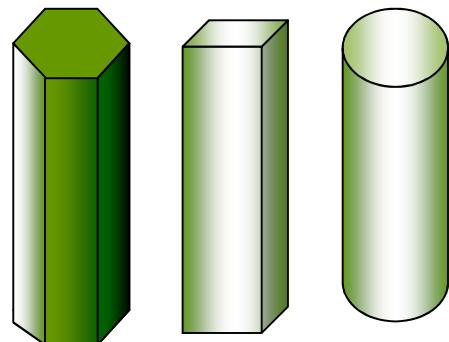


$$e_K = K_1' \sin^2 \theta + K_2' \sin^4 \theta$$



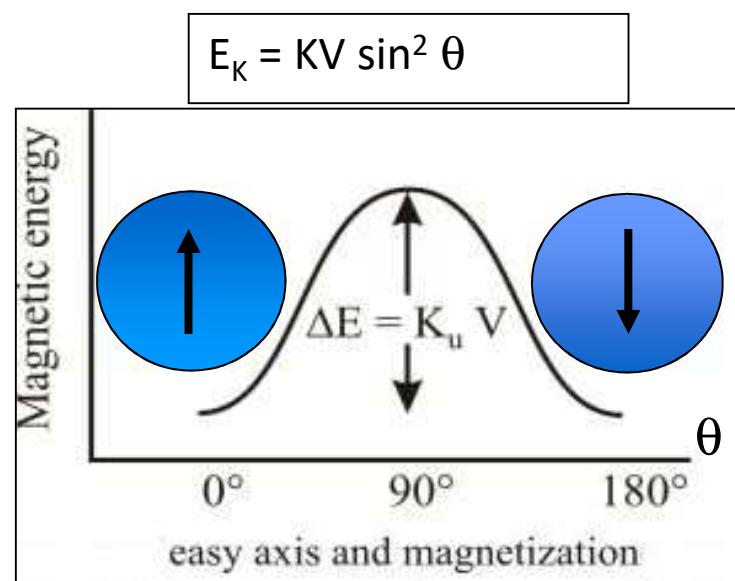
energía de anisotropía (E_K)

Anisotropía uniaxial



$$e_K = K_1 \sin^2 \theta + K_2 \sin^4 \theta \longrightarrow e_K = K \sin^2 \theta$$

Siempre que
pueda simplificarse



Anisotropía uniaxial

ejemplos

$$e_K = K_1 \sin^2 \theta + K_2 \sin^4 \theta$$

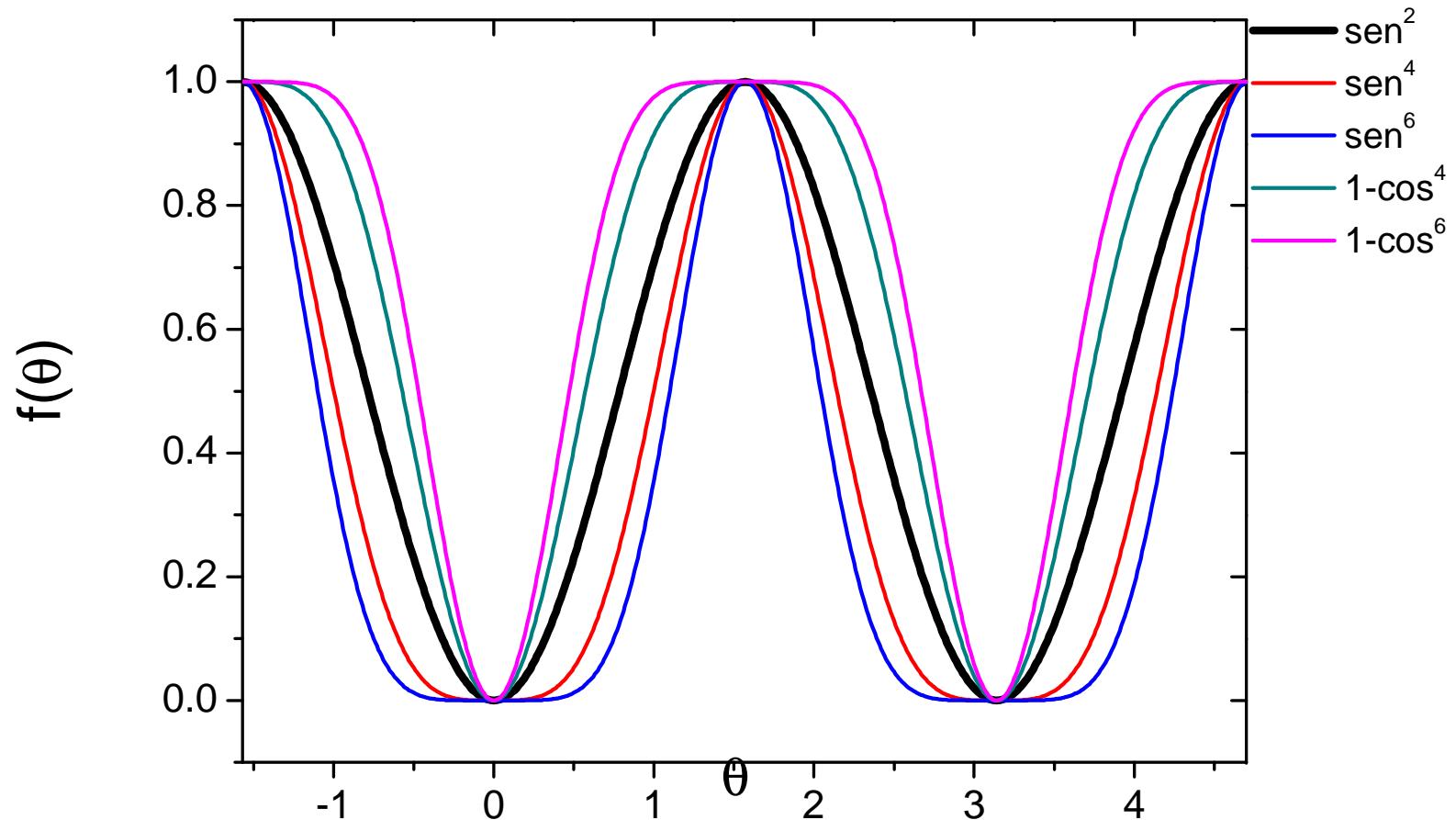
Material	K_1 (10^5 J/m ³)	K_2 (10^5 J/m ³)	Eje fácil
Co	4.1	1.0	hexagonal
SmCo_5	1100	-	hexagonal

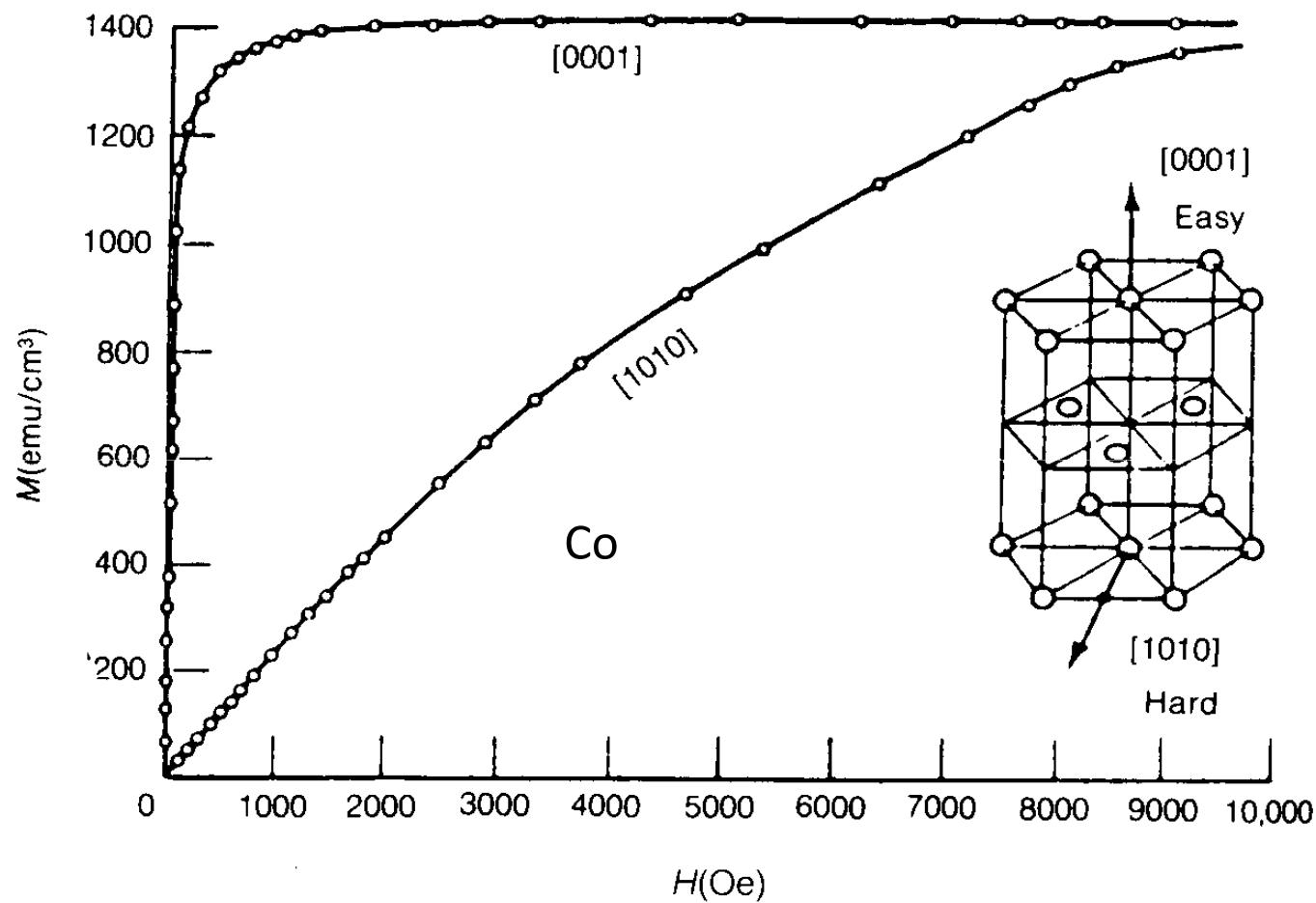
Anisotropía uniaxial

Efecto de las potencias de seno y coseno

$$e_K = K \sin^n \theta$$

$$e_K = K(1 - \cos^n \theta)$$



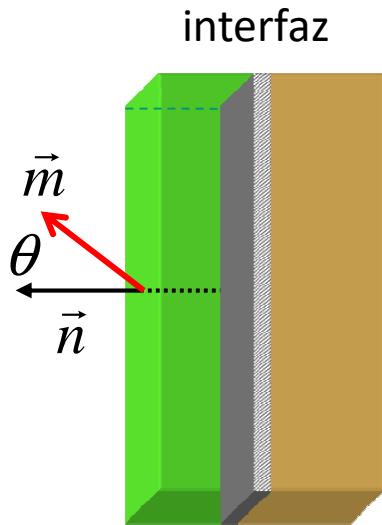


Anisotropía de Interfaz

Anisotropía de Intercambio

superficies e interfaces

Anisotropía de interfaz



$$\vec{m} = \vec{M} / M$$

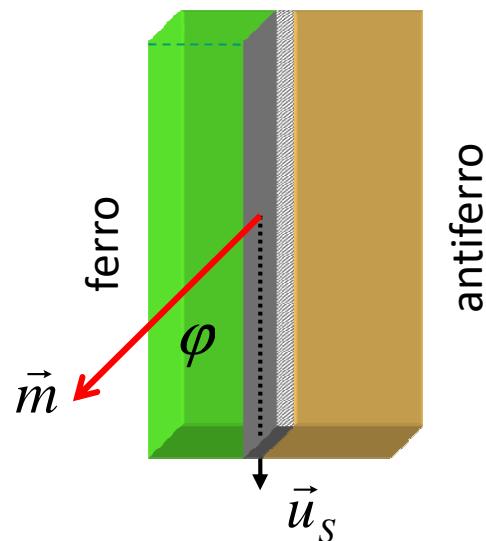
$$e_K = K_S [1 - (\vec{m} \cdot \vec{n})^2]$$

$$(e_K = K_S [1 - (\cos \theta)^2])$$

$K_S > 0 \Rightarrow \vec{m} \parallel \text{sup}$

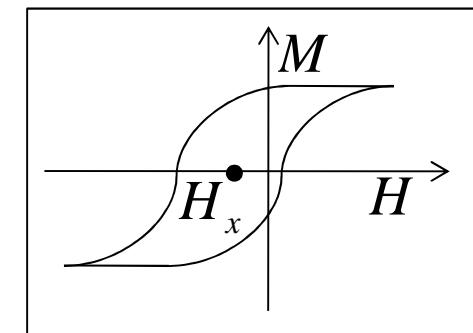
$K_S < 0 \Rightarrow \vec{m} \perp \text{sup}$

Anisotropía de intercambio*



$$e_K = K_S \vec{m} \cdot \vec{u}_S = \frac{H_x}{2} \vec{m} \cdot \vec{u}_S$$

$$e_K = \frac{H_x}{2} m \cos \phi$$



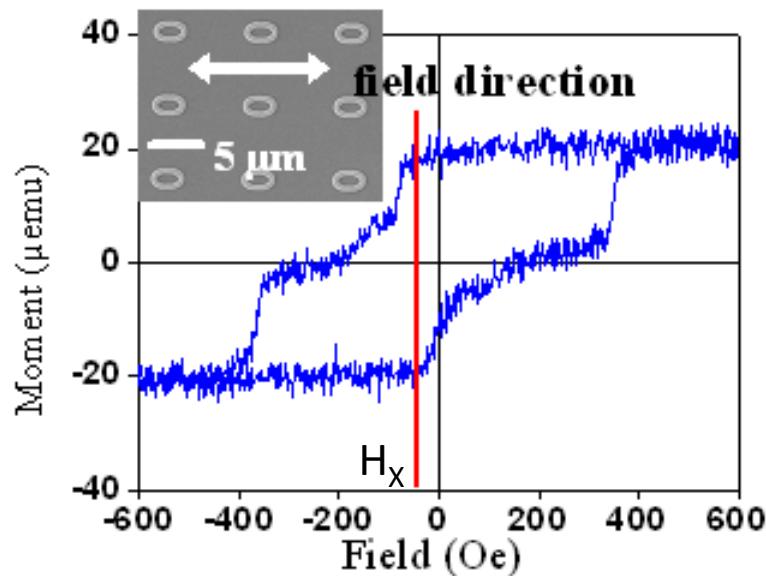
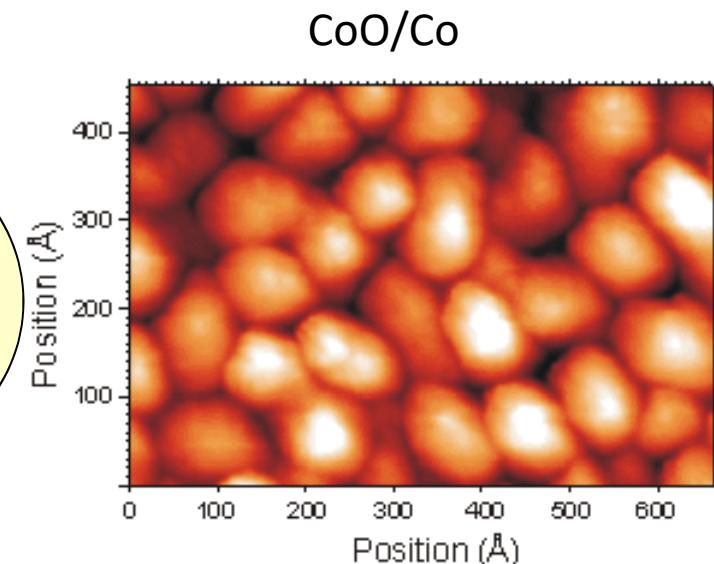
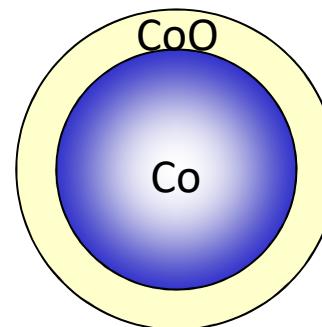
Exchange bias field

*también llamada unidireccional

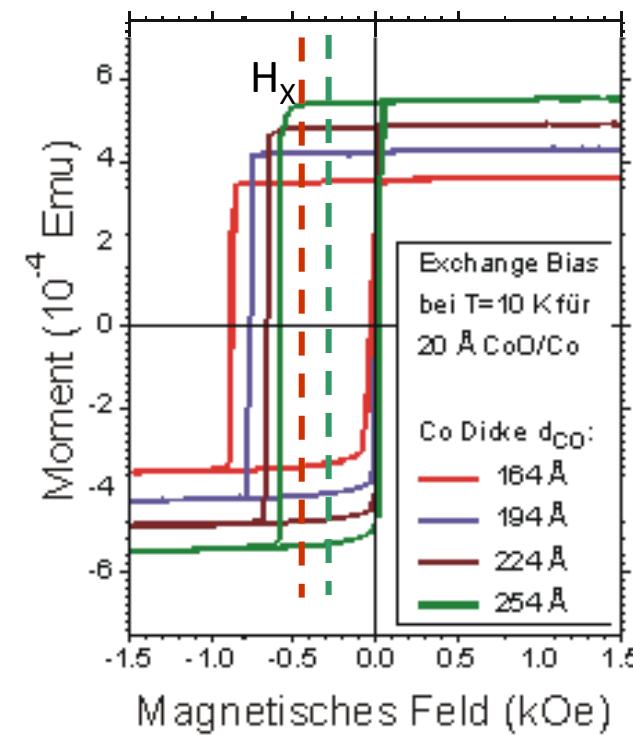
Anisotropía de intercambio

Observación del exchange bias

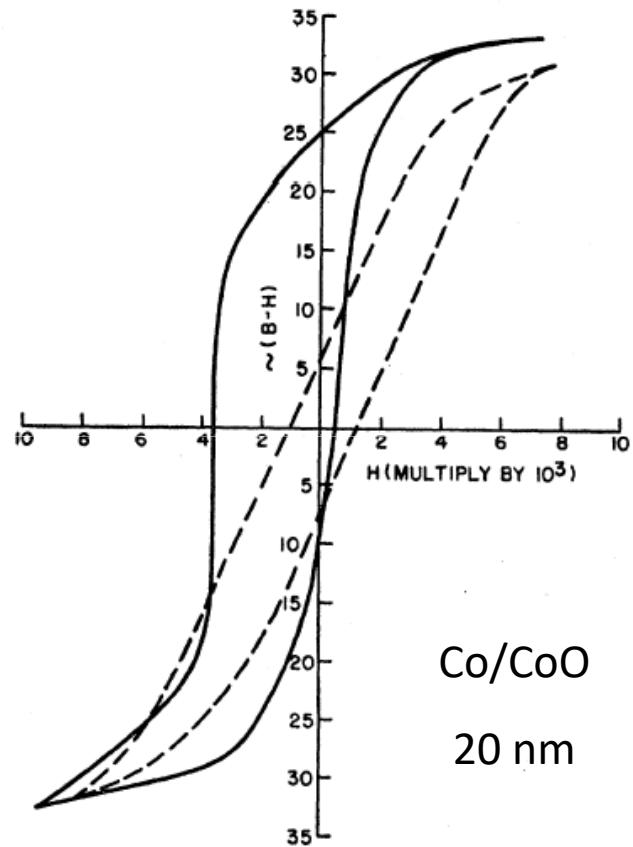
$$e_K = K_S \vec{m} \cdot \vec{u}_S = \frac{H_x}{2} \vec{m} \cdot \vec{u}_S$$



Ta 20nm / NiFe 20nm/ FeMn 10 nm film



In the
news... 



Letters to the Editor

New Magnetic Anisotropy

W. H. MEIKLEJOHN AND C. P. BEAN

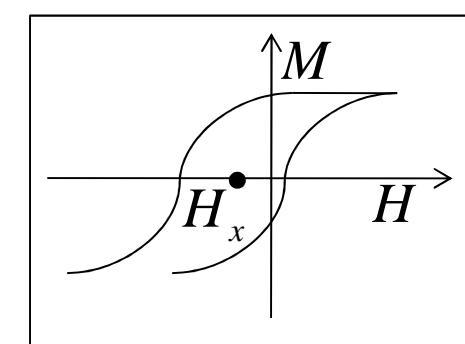
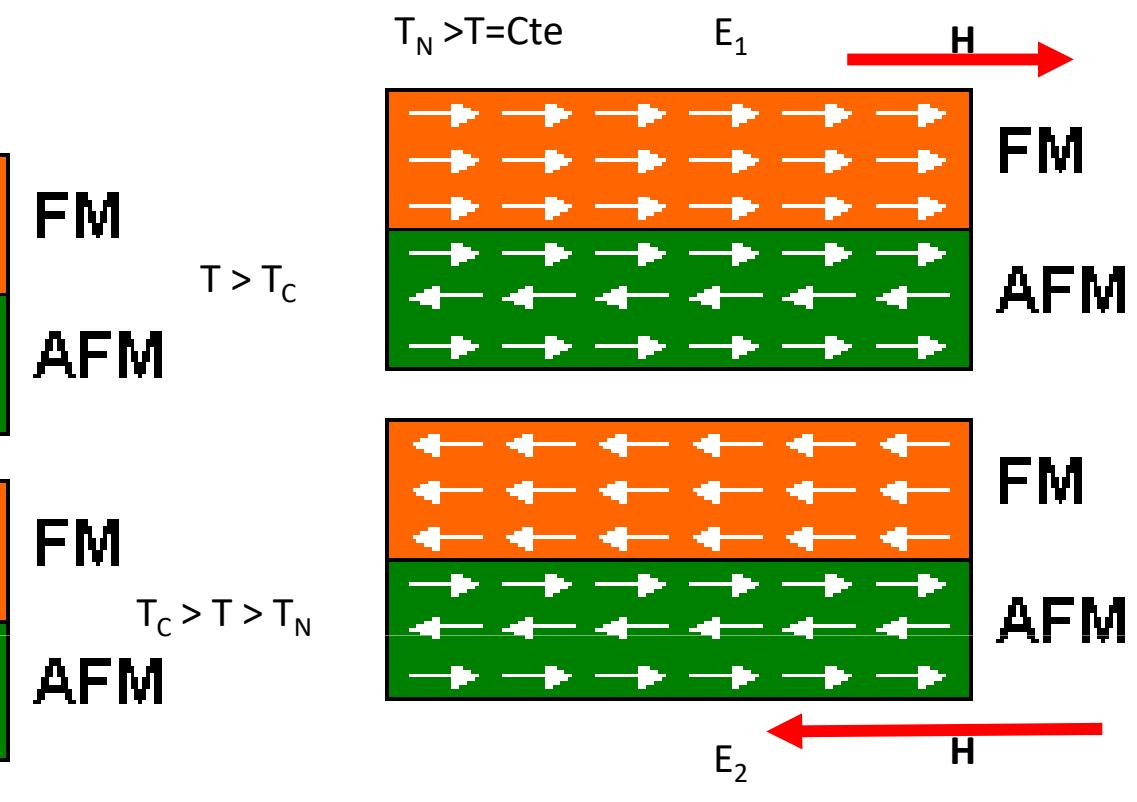
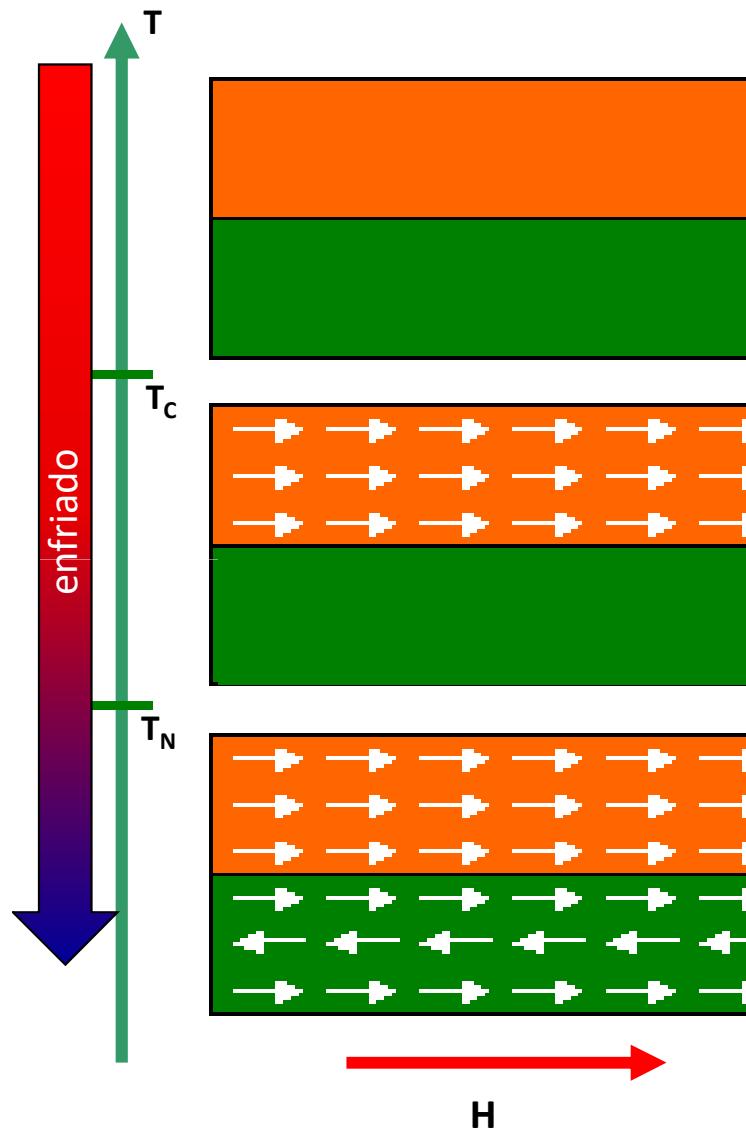
General Electric Research Laboratory, Schenectady, New York

(Received March 7, 1956)

PHYSICAL REVIEW

VOLUME 102, NUMBER 5

JUNE 1, 1956

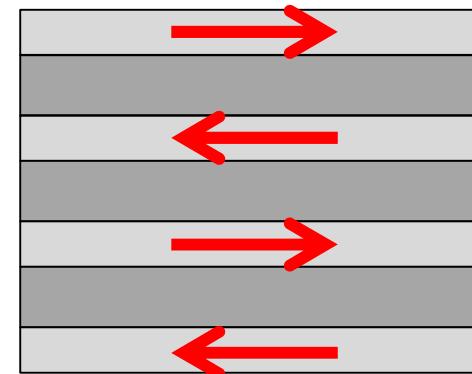
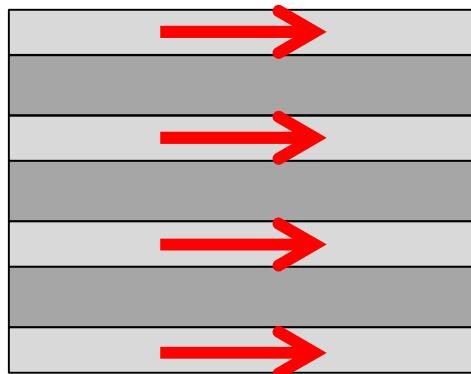


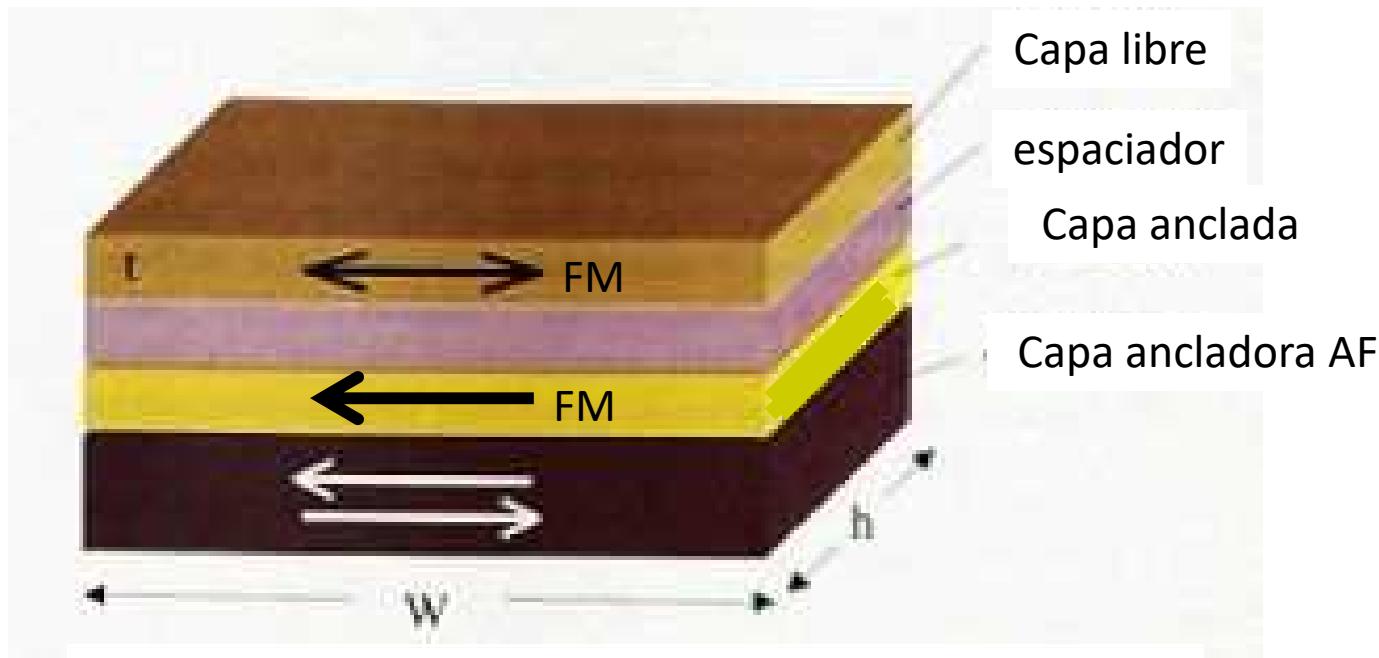
Magnetoresistencia

baja resistencia

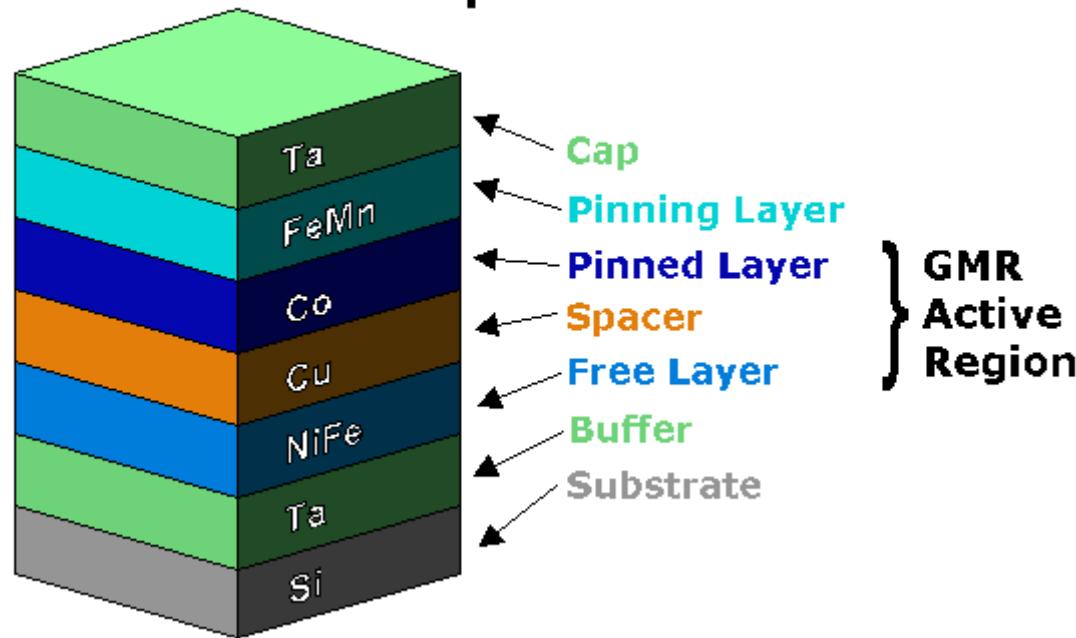


alta resistencia

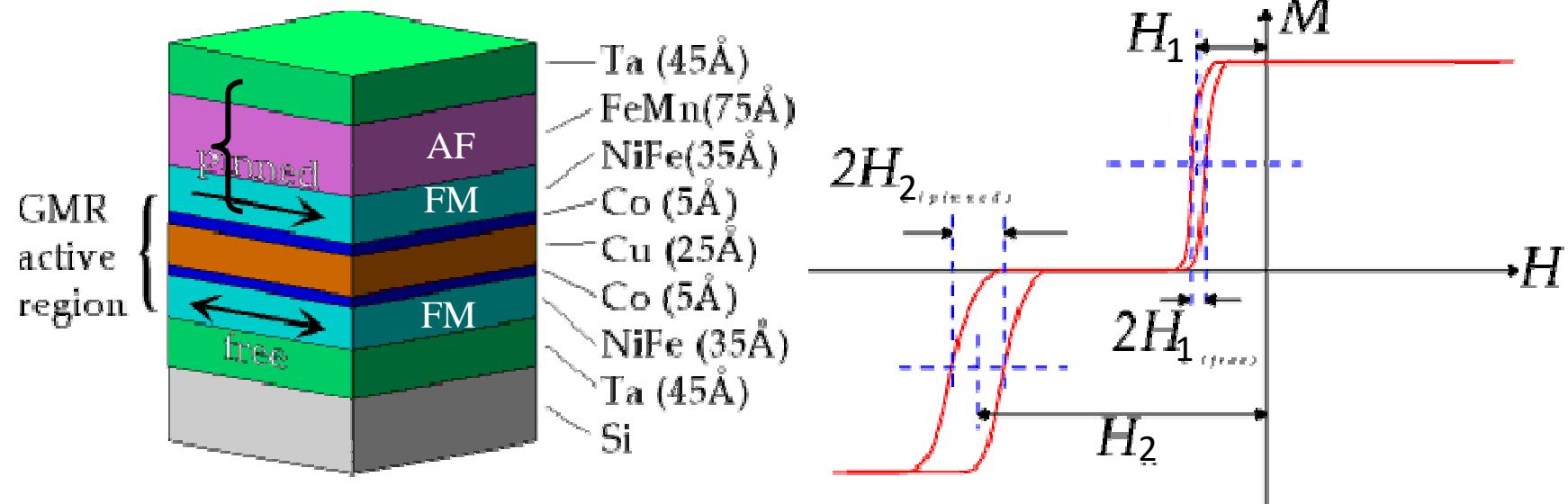




Spin Valve Structure

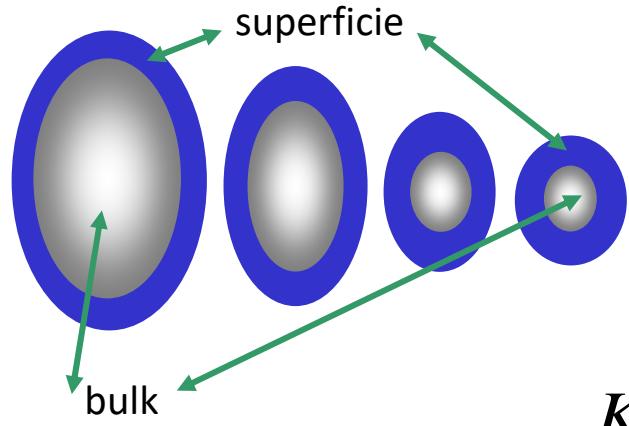


Válvula de spin



Anisotropía en nanopartículas magnéticas

anisotropía de superficie en nanopartículas



$$K_{ef} = K_B + K_{V_S}^{ef}$$

|

$$K_{V_S}^{ef} \approx \frac{SK_S}{V} \approx \frac{4\pi r^2}{\frac{4}{3}\pi r^3} K_S = \frac{3}{r} K_S = \frac{6}{d} K_S$$

Partícula esférica

superficies/interfaces:

- discontinuidad composicional y configuracional
- mayor efecto anisotrópico

$$K_{ef} = K_B + \frac{6K_s}{d}$$

↓

$$K_{ef} = K_B + \gamma \frac{K_s}{d}$$

Bødker et. Al (1994)

Anisotropía de superficie - ejemplo

$$K_B(Co_{fcc}) \approx 1 \times 10^5 J/m^3$$

$$K_S(Co / Al_2O_3) \approx 3.3 \times 10^{-4} J/m^2$$

$$K_{ef} = K_B + \gamma \frac{K_s}{d}$$

$$K_{ef}(Co / Al_2O_3) \approx \left[1 \times 10^5 + 6 \frac{3.3 \times 10^{-4}}{11 \times 10^{-9}} \right] J/m^3 \approx 2.8 \times 10^5 J/m^3$$

Si $d \sim 3 \text{ nm} = 3 \times 10^{-9} \text{ m}$



$$K_{ef}(Co / Al_2O_3) \approx 10^6 J/m^3$$

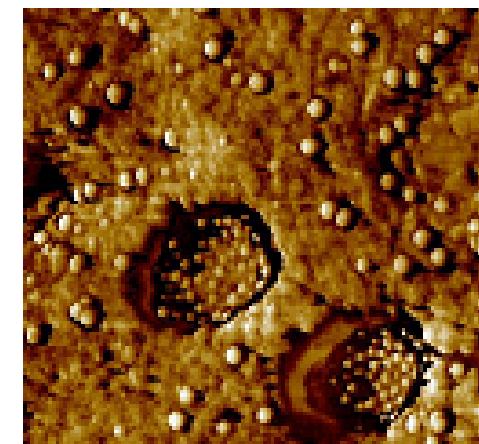
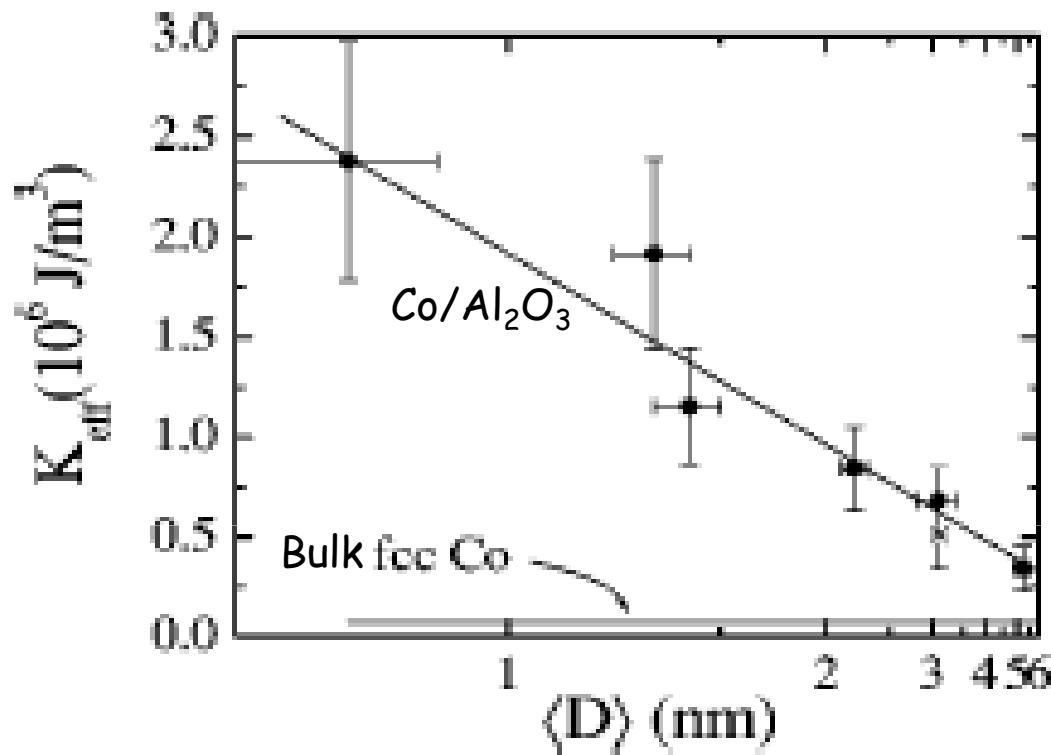


Imagen MFA de nanopartículas de Co fcc en una matriz de alúmina. Las partículas son de aprox 11 nm (diámetro).

$$\tau = \tau_0 e^{\frac{K_{ef}V}{kT}}$$

Mayores tiempos de relajación



F. Luis, J.M. Torres, L.M. Gracia, J. Bartolomé, J. Stankiewicz, F. Petroff, F. Fettar, J. L. Maurice and A. Vaurés. Phys. Rev B, **65** (2002) 094409

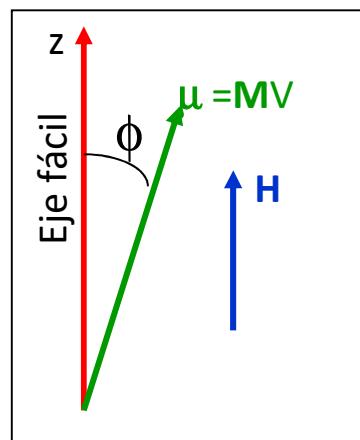
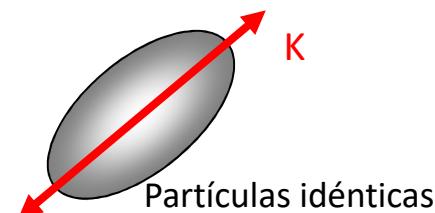
Modelo de Stoner - Wohlfarth

$$T = 0K$$

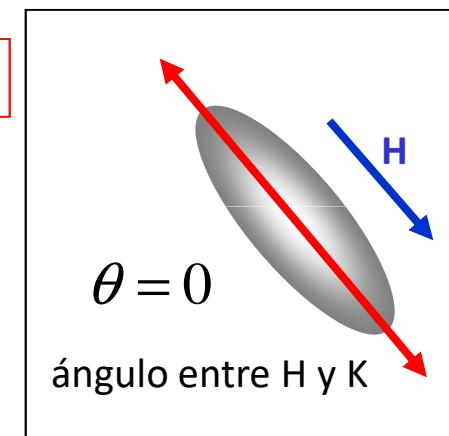
monodominio

Anisotropía uniaxial

no interactuantes



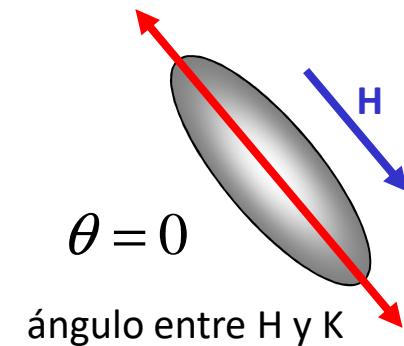
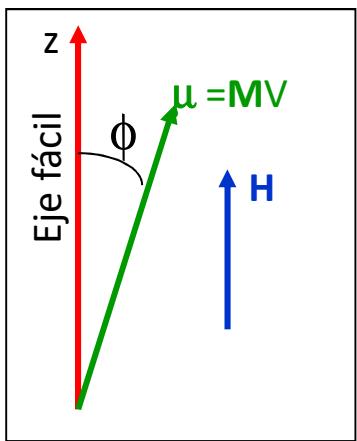
Campo paralelo al eje fácil



$$E_K = e_K V = KV \sin^2 \phi$$

$$E_H = -\vec{\mu} \cdot \vec{B} = -\mu_0 \vec{\mu} \cdot \vec{H} = -\mu_0 V M_z H = -\mu_0 V M_s H \cos \phi$$

$$E = E_K + E_H = KV \sin^2 \phi - \mu_0 V M_s H \cos \phi$$

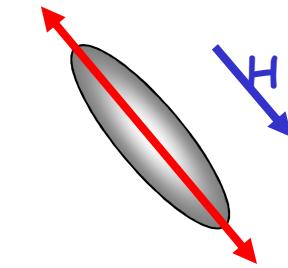


$$E = E_K + E_H = KV \sin^2 \phi - \mu_0 V M_s H \cos \phi$$

llamamos Campo de anisotropía

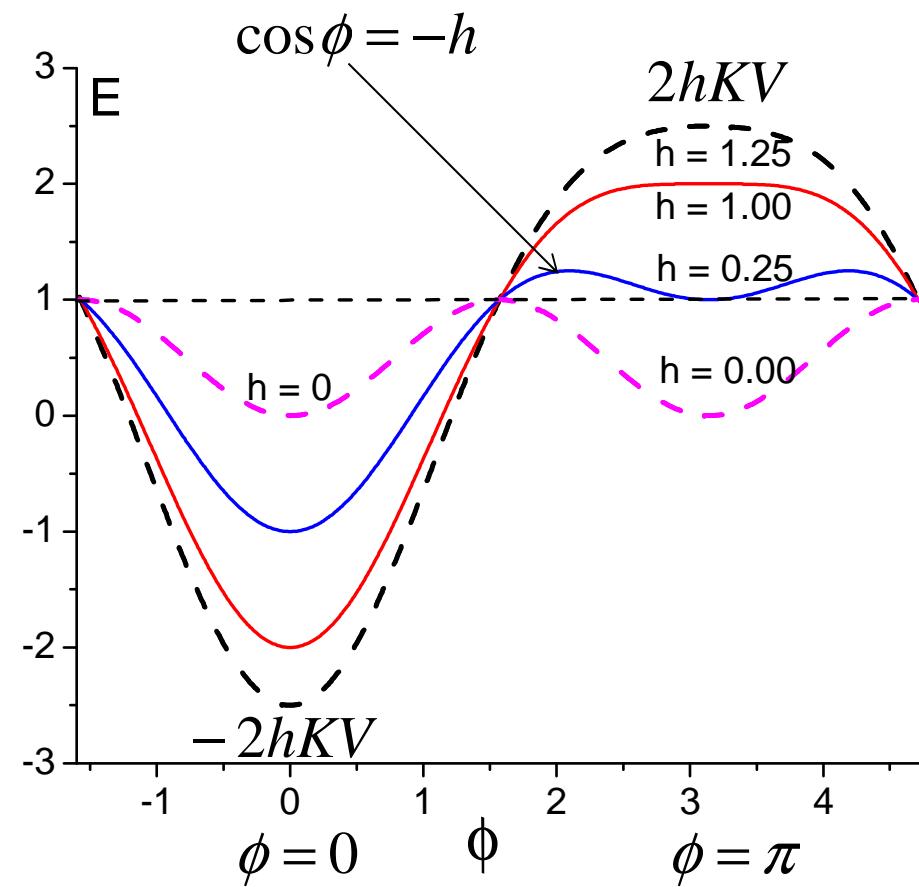
$$H_K = \frac{2K}{\mu_0 M_s} \quad h = \frac{H}{H_K} = \frac{\mu_0 M_s H}{2K}$$

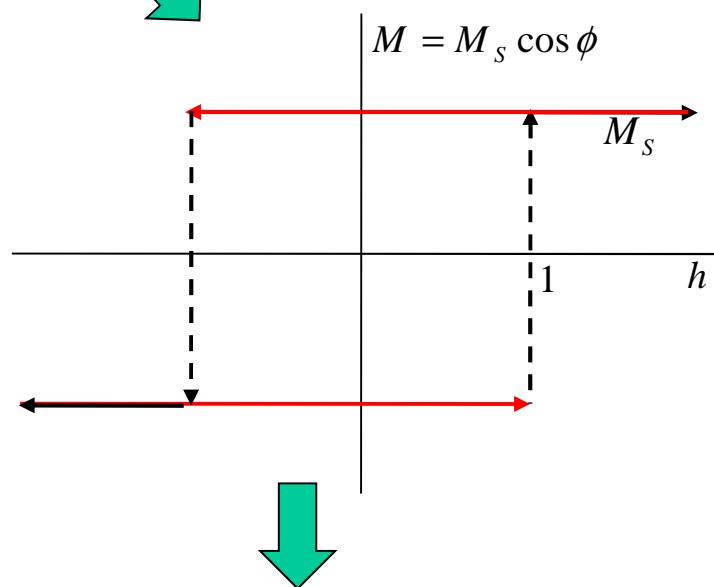
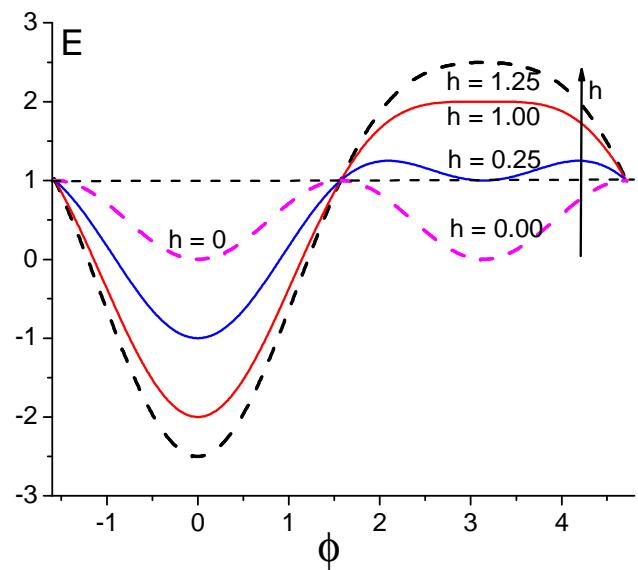
$$E = KV (\sin^2 \phi - 2h \cos \phi)$$

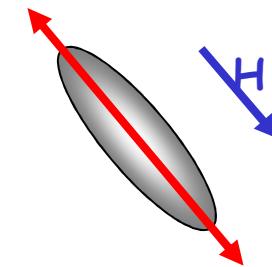


$$E = KV \left(\sin^2 \phi - 2h \cos \phi \right)$$

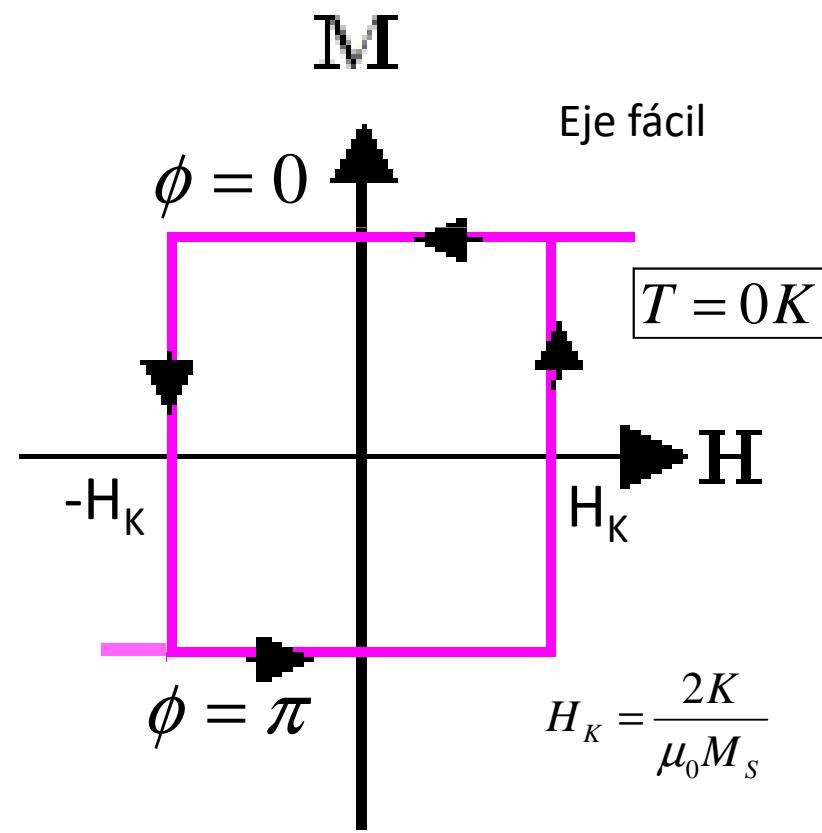
$$h = \frac{H}{H_K} \quad H_K = \frac{2K}{\mu_0 M_s}$$





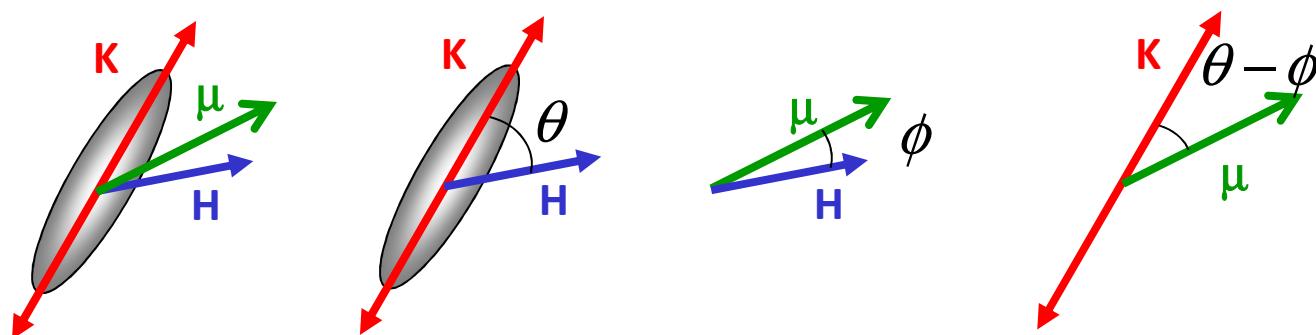


$$M_z = M_s \cos \theta$$

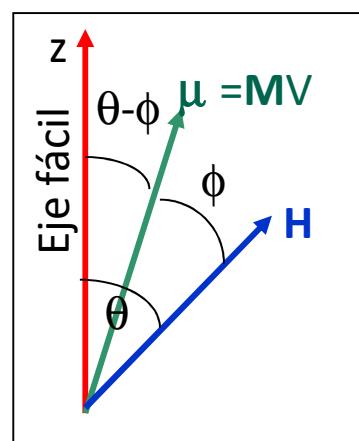


Campo en dirección arbitraria

$$\theta \neq 0$$

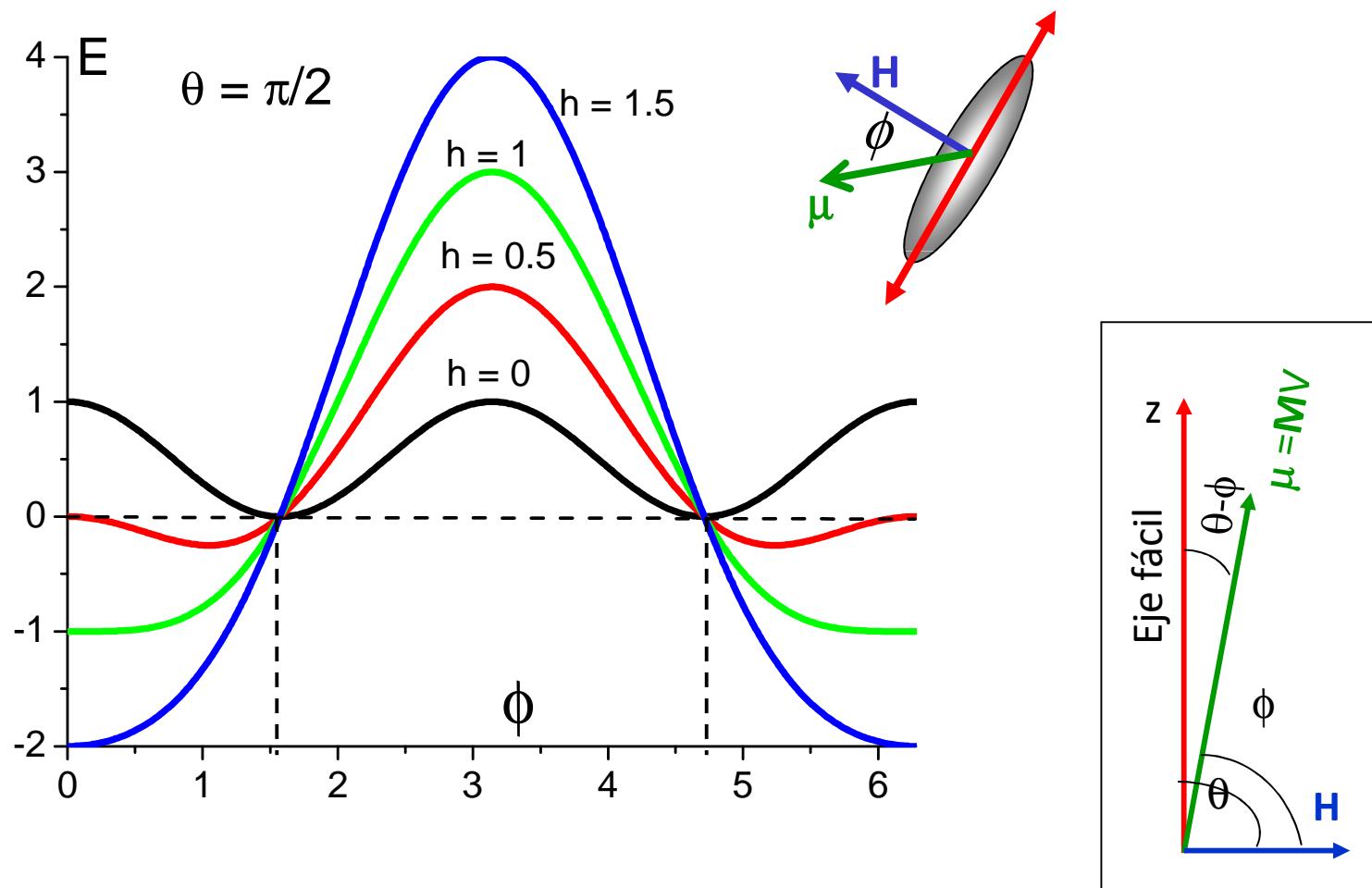


$$E = E_K + E_H = KV[\sin^2(\phi - \theta) - 2h\cos\phi]$$

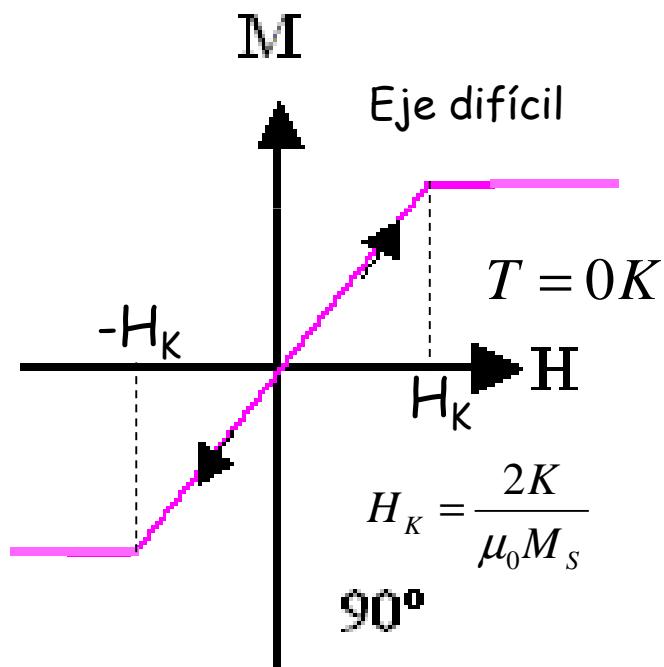
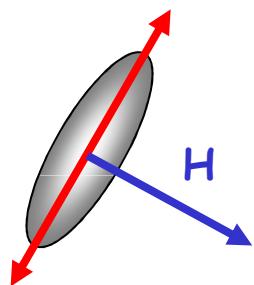


$$\theta = \pi / 2$$

$$E = E_K + E_H = KV \cos \phi (\cos(\phi) - 2h)$$

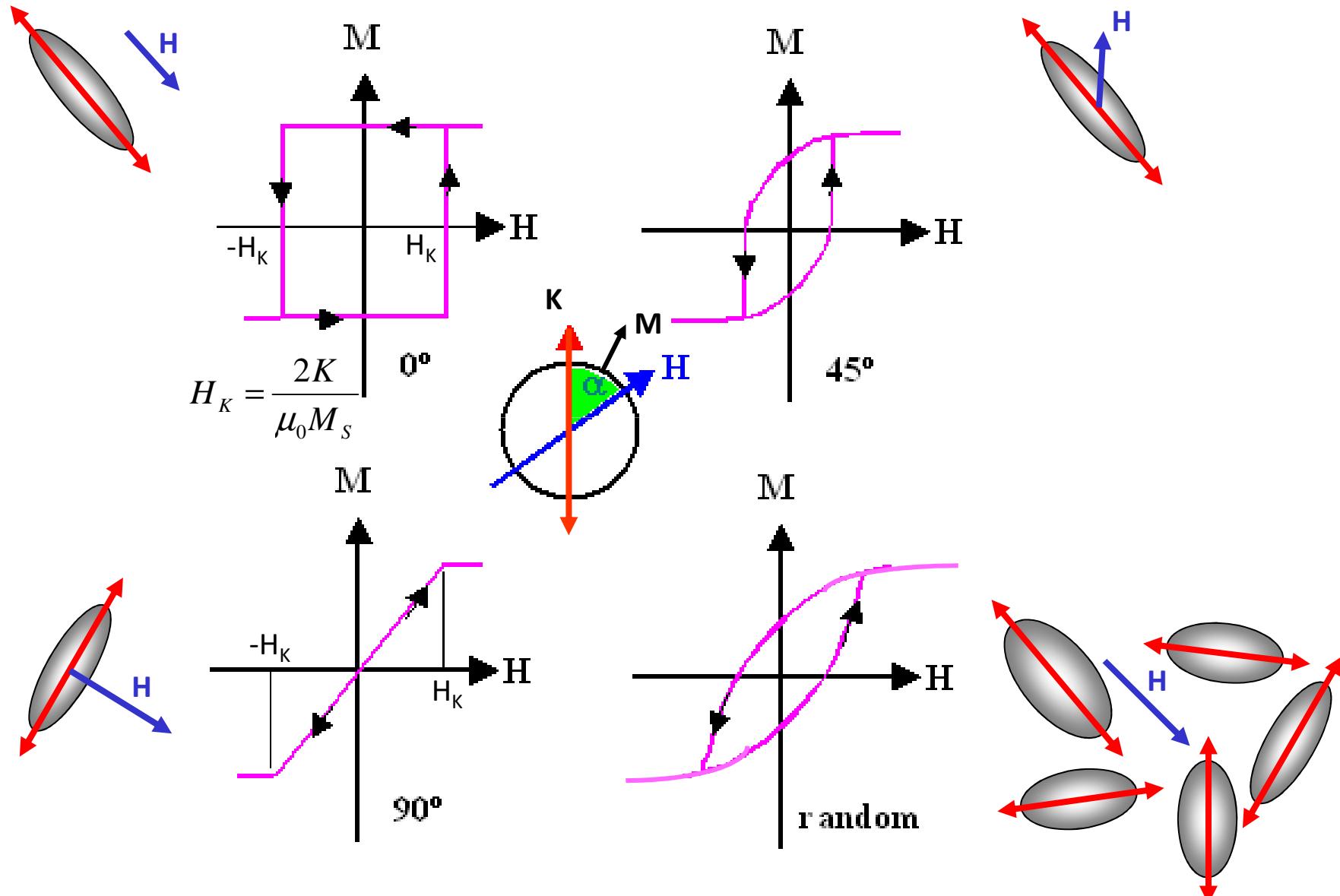


$$M_z = \frac{M_s}{H_K} H; \quad |h| < 1$$



Partículas ferromagnéticas pequeñas – modelo de Stoner - Wohlfarth

régimen bloqueado $\rightarrow T = 0 \text{ K}$



E.C. Stoner y E.P. Wohlfarth, IEEE Transactions on Magnetics **27**, 3475-3518 (1991)

[599]

A MECHANISM OF MAGNETIC HYSTERESIS IN
HETEROGENEOUS ALLOYS

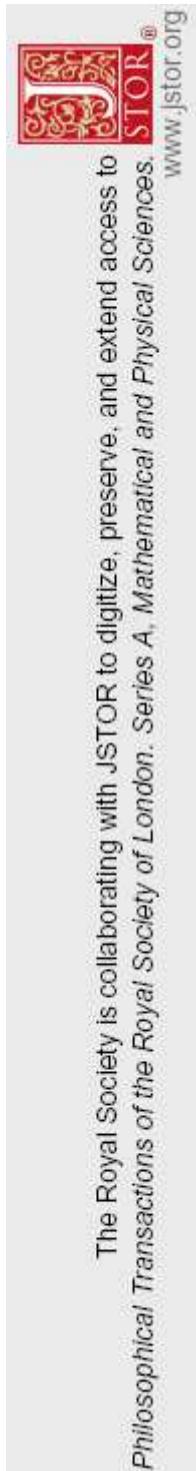
BY E. C. STONER, F.R.S. AND E. P. WOHLFARTH
Physics Department, University of Leeds

(Received 24 July 1947)

VOL. 240. A. 826 (Price 10s.)

74

[Published 4 May 1948]



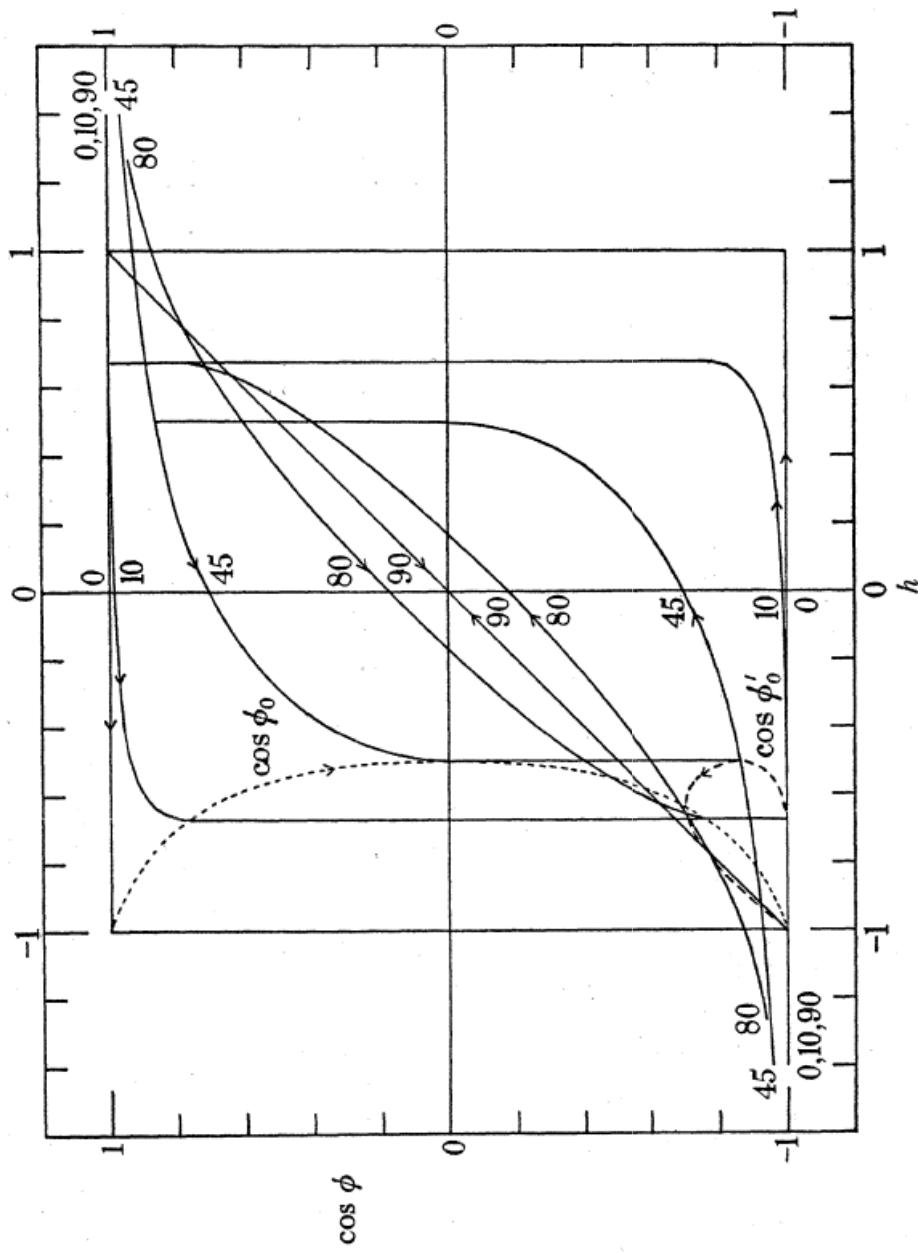


FIGURE 6. Magnetization curves for prolate spheroids. The resolved magnetization in the positive field direction is given by $I_0 \cos \phi$, where I_0 is the saturation magnetization. The field, H , is given by $H = (N_b - N_a) I_0 h$, where N_a and N_b are the demagnetization coefficients along the polar and equatorial axes. The angle, θ , between the polar axis and the direction of the field, is shown, in degrees, by the numbers on the curves. The dotted curves give $\cos \phi_0$ and $\cos \phi'_0$, where ϕ_0 and ϕ'_0 are the angles made with the positive field direction by the magnetization vector at the beginning and end of the discontinuous change at the critical value, h_0 , of the field.

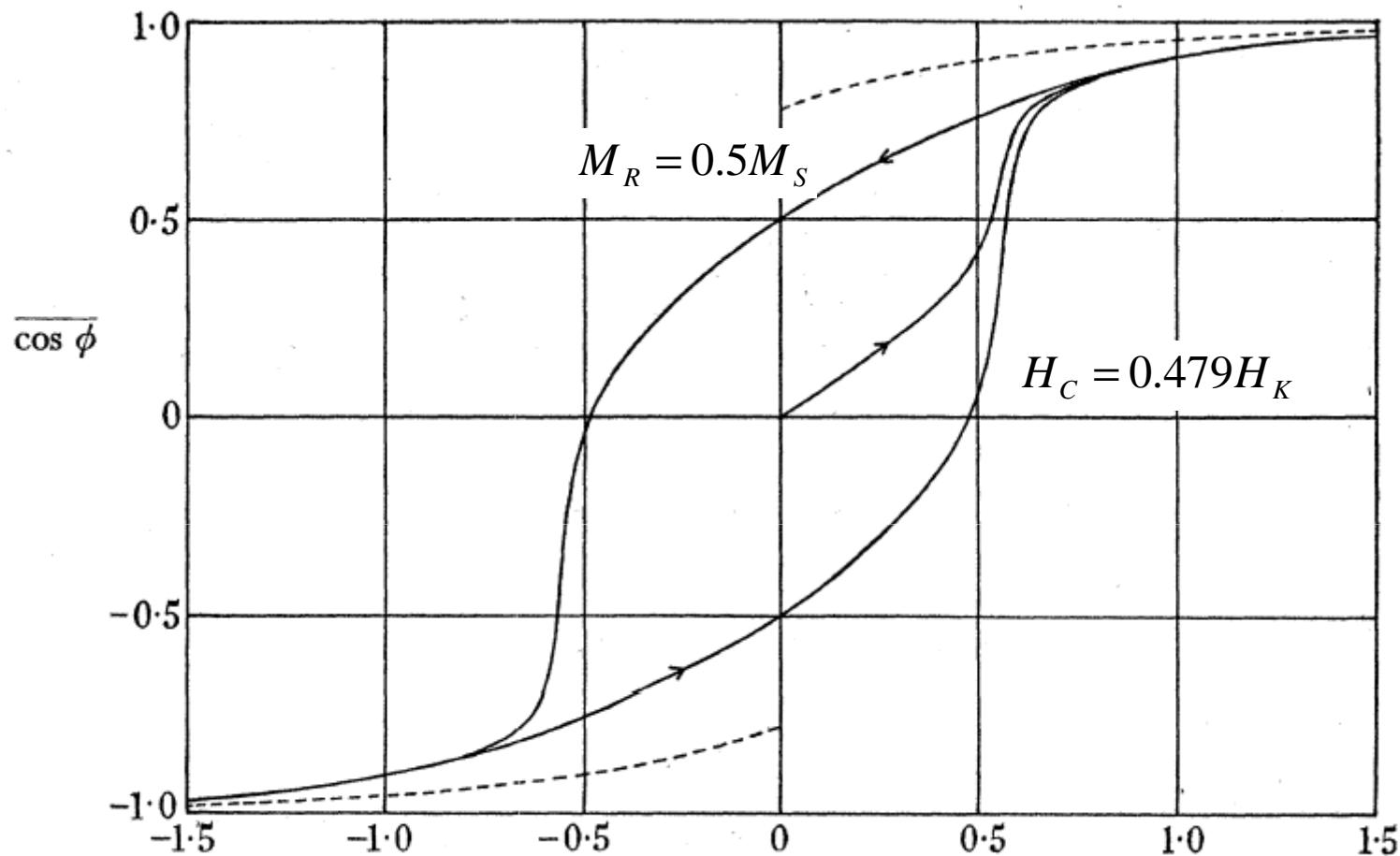


FIGURE 7. Magnetization curves for prolate (full curves) and oblate (broken curves) spheroids orientated at random. The curves refer to similar prolate (or oblate) spheroids orientated at random. $\cos \phi$ is proportional to the mean resolved magnetization per spheroid in the positive field direction, or to the resultant magnetization in this direction of the assembly, $H = (|N_a - N_b|) I_0 h$.

Rapid-turnaround characterization methods for MRAM development

by D. W. Abraham,
P. L. Trouilloud,
and D. C. Worledge

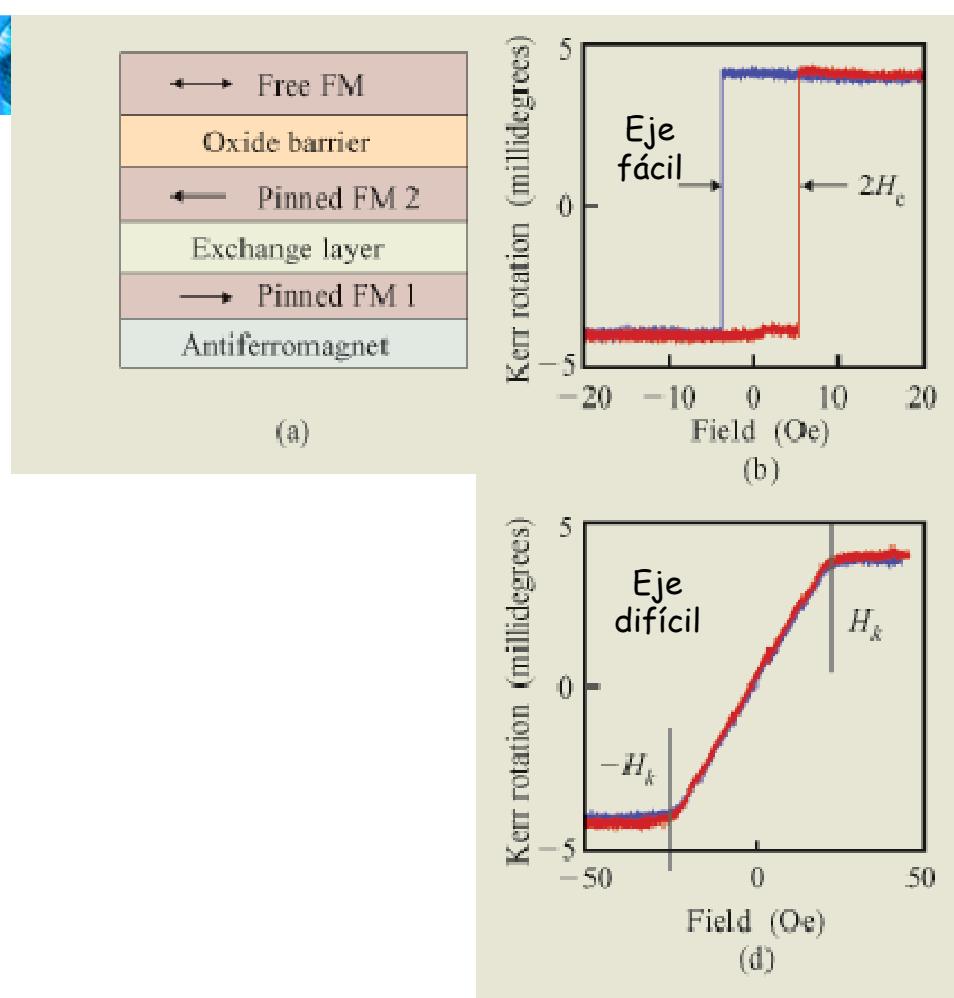
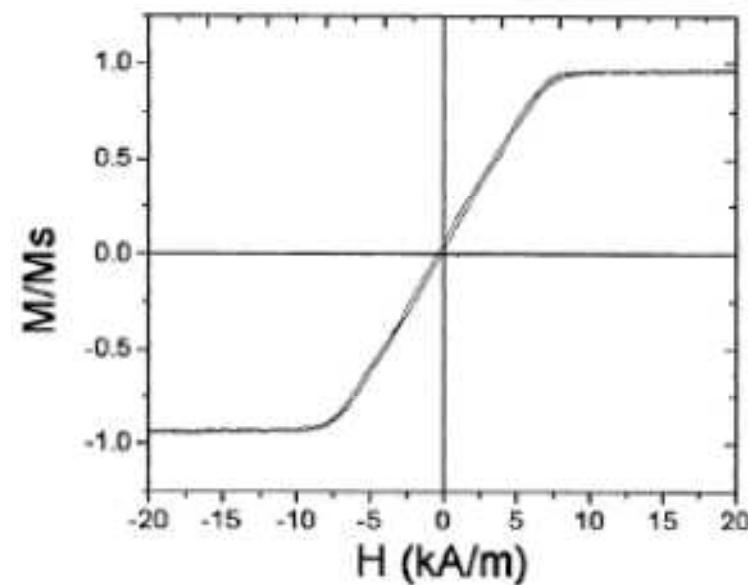
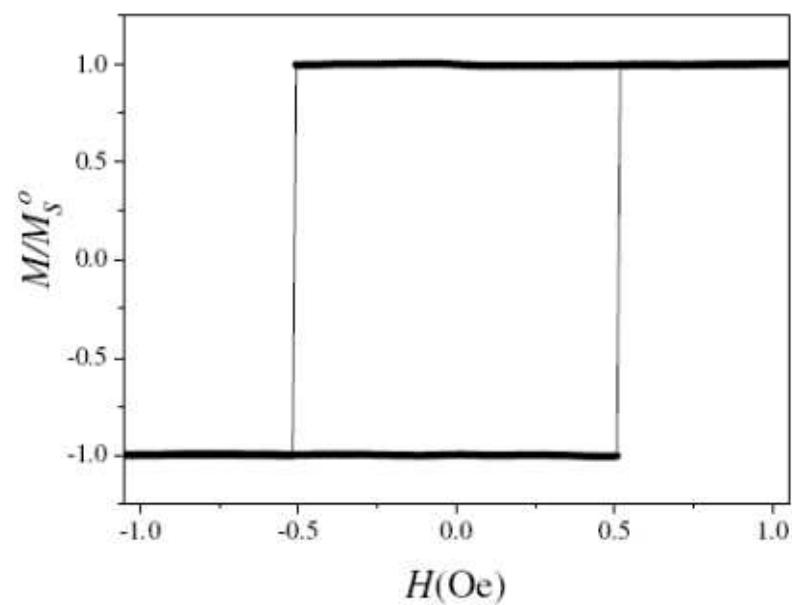
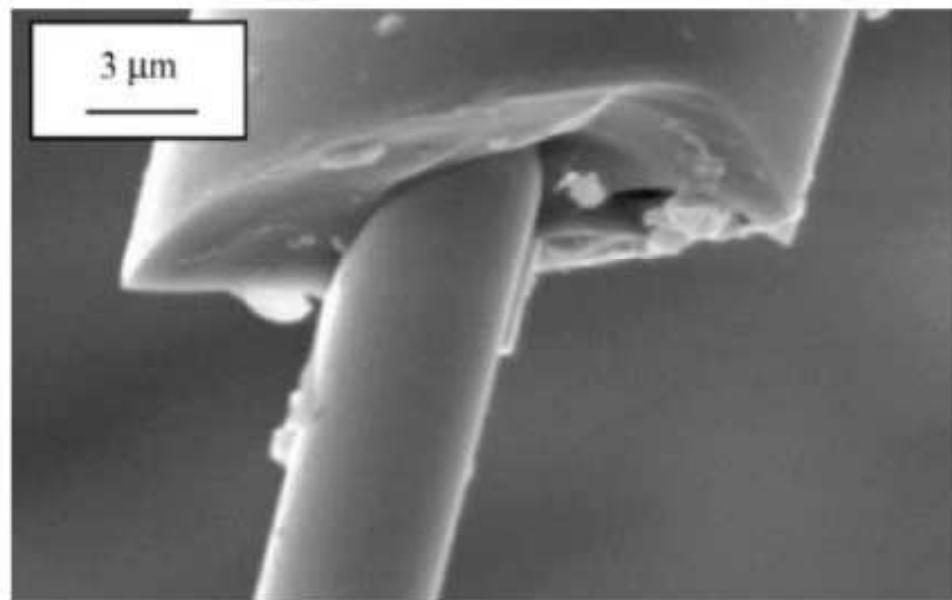


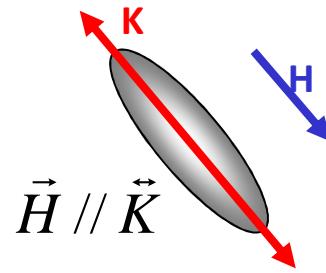
Figure 4

(a) Typical data for a Stoner–Wohlfarth stack. (a) Kerr easy-axis (EA) data taken at low field, showing the excellent low Néel offset and sharp hysteresis loop. (c) High-field EA Kerr magnetometry data showing the relative motion of the magnetization in the two ferromagnetic films, permitting direct measurement of pinning and interlayer coupling. (d) Hard-axis data revealing the film anisotropy.

Microhilos, P. Mendoza Zéliz et al, 2007



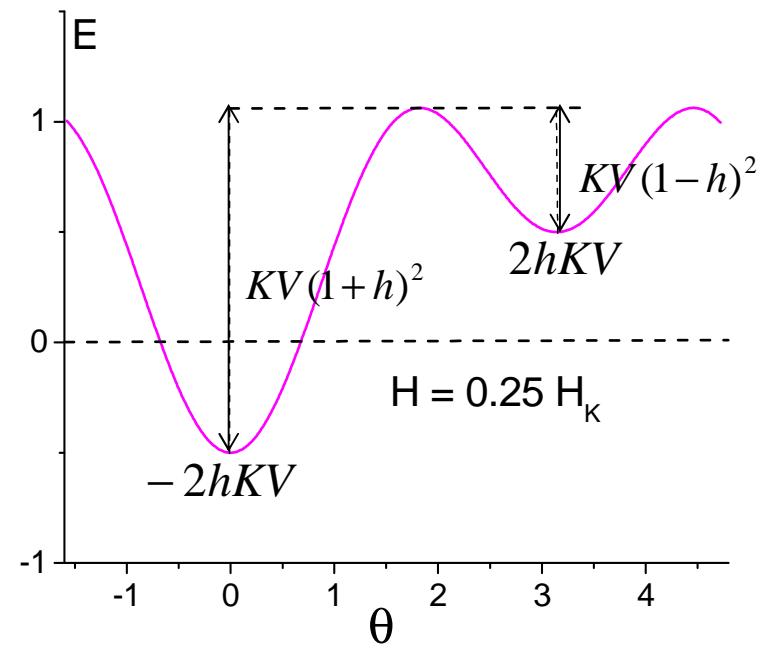
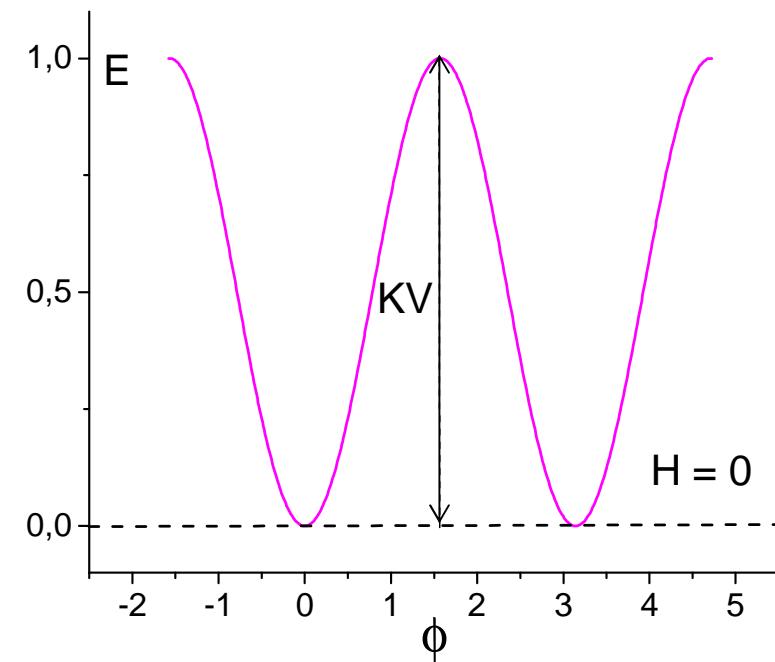
Efectos Dinámicos ($T \neq 0$)

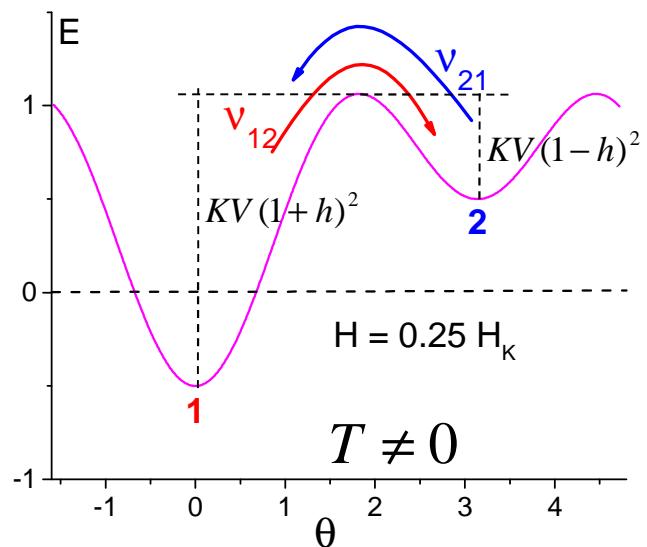


$$E = KV(\sin^2 \phi - 2h \cos \phi)$$

$$h = \frac{H}{H_K}$$

$$H_K = \frac{2K}{\mu_0 M_s}$$





$$\Delta E_{ij} = KV(1+h)^2$$

$$v_{ij} = c_0 e^{-\frac{\Delta E_{ij}}{kT}}$$

Frecuencia de saltos

$$\tau_{ij} = c_0^{-1} e^{\frac{\Delta E_{ij}}{kT}}$$

$$\xrightarrow{T=0} v_{ij} = 0$$

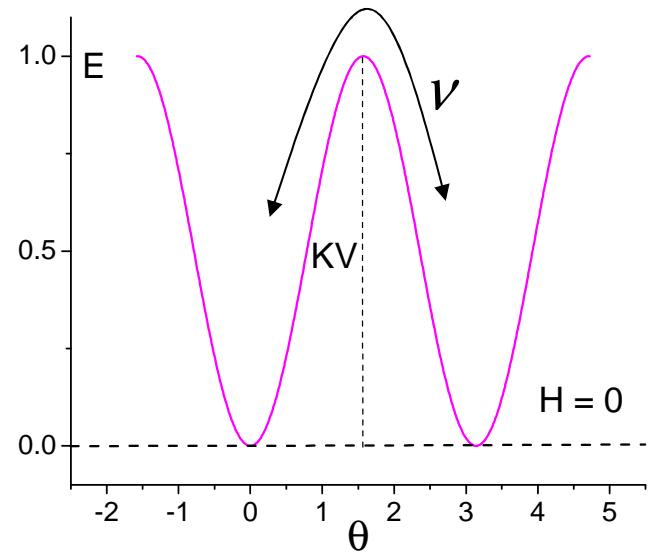
$$\xrightarrow{T=\infty} v_{ij} = c_0$$

Frecuencia de intentos

Tiempo de relajación

$$\tau_{ij} = c_0^{-1} e^{\frac{\Delta E_{ij}}{kT}}$$

Tiempo de
relajación



Para $H = 0$

$$\nu_{12} = \nu_{21} = \nu$$

$$\nu = \nu_0 e^{-\frac{KV}{kT}}$$



$$\tau = \tau_0 e^{\frac{KV}{kT}}$$

$$\tau_0 = c_0^{-1}$$

$$10^{-12} s \leq \tau_0 \leq 10^{-8} s$$

$$\tau = \tau_0 e^{\frac{KV}{kT}}$$

$$\tau_0 \approx cte$$

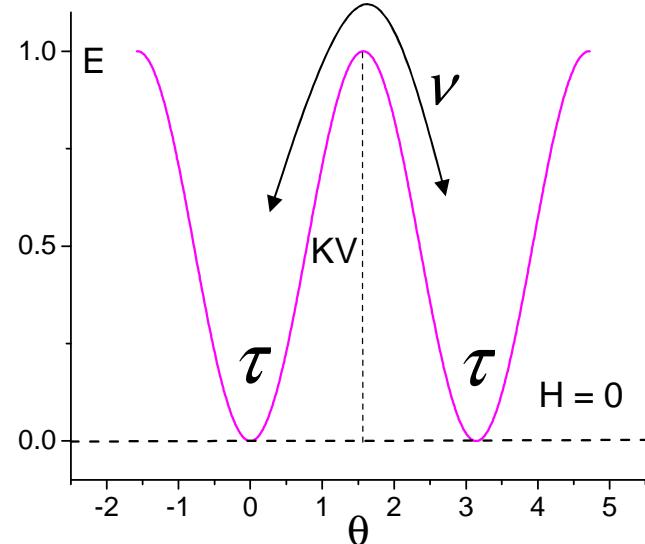
Ejemplo, usando $\tau_0 = 10^{-9}$ s

material	K(J/m ³)	R(nm)	τ (s)
Co	3.9×10^5	4.4	6×10^5
		3.6	0.1
Fe	4.7×10^4	14.0	1.5×10^5
		11.5	0.07

Comportamiento superparamagnético

Tiempo Experimental vs Tiempo de Relajación

$$\tau = \tau_0 e^{\frac{KV}{kT}}$$

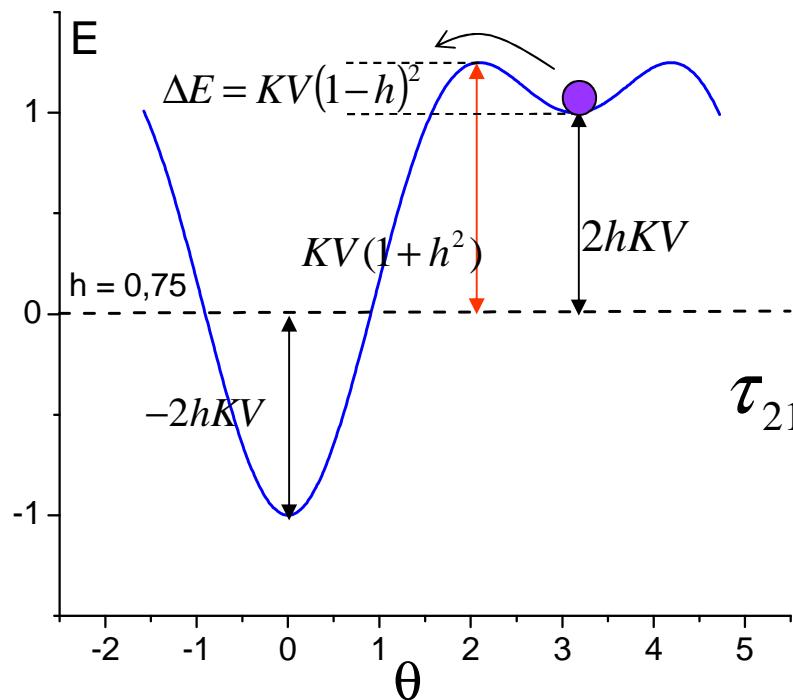


Técnica	τ_{exp}
Mössbauer $^{57}\text{Fe}, ^{119\text{m}}\text{Sn}$	$\approx 10^{-8}\text{s}$
Susceptibilidad ac	$10^{-4} - 1\text{ s}$
Susceptibilidad $ac hf$	desde 10^{-6} s
Magnetización dc	$0.1 - 100\text{ s}$

$\tau_{\text{exp}} < \tau \leftrightarrow T < T_B$	Sistema bloqueado	Patrón estático	Histéresis, desdoblamiento Zeeman (EM)
$\tau_{\text{exp}} > \tau \leftrightarrow T > T_B$	Sistema desbloqueado	Patrón dinámico	Equilibrio, patrón super- paramagnético (EM)

Dependencia del campo coercitivo con la temperatura

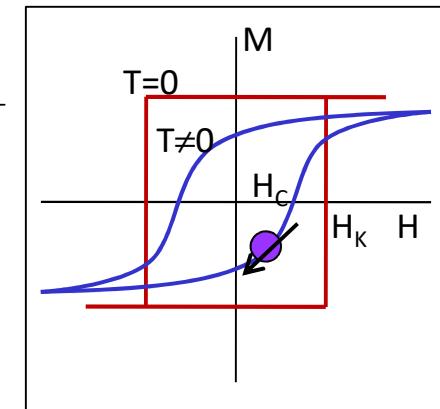
$$h = H / H_K = \frac{\mu_0 M_S H}{2K}$$



$$H_C = H_K = \frac{2K}{\mu_0 M_S}$$

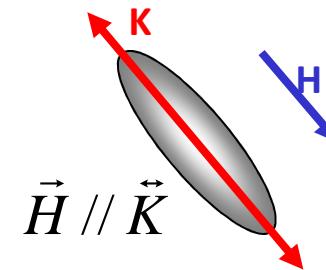
$$\tau_{21} = \tau_0 e^{-\frac{KV(1-h)^2}{kT}}$$

a $T \neq 0$ K la inversión de M se producirá cuando $\tau_{21} \approx \tau_{\text{exp}}$



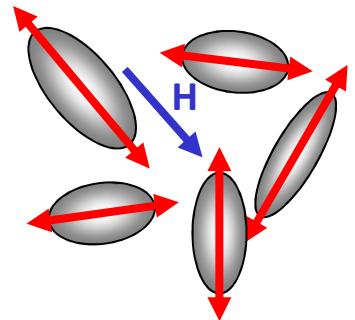
Dependencia del campo coercitivo con la temperatura

$$H_C(T) \approx H_K \left(1 - \sqrt{\frac{kT}{KV} \ln(\tau_{\text{exp}} / \tau_0)} \right)$$

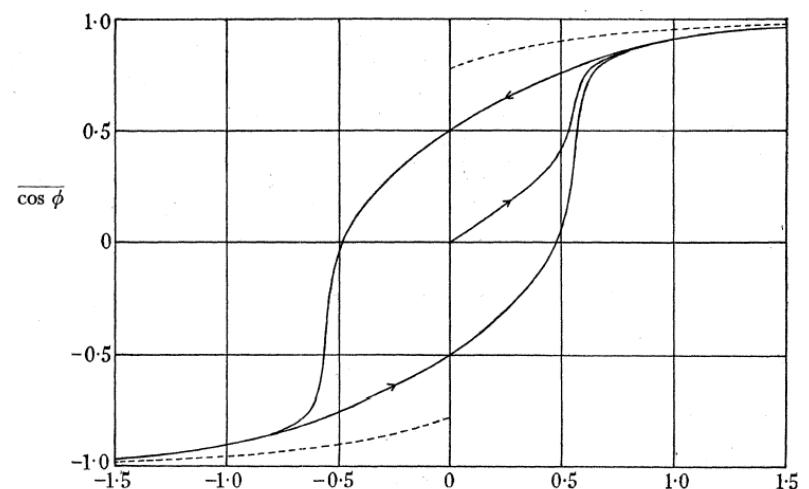


orientación aleatoria

$$H_C(T) \approx 0.48 H_K \left(1 - \sqrt{\frac{kT}{KV} \ln(\tau_{\text{exp}} / \tau_0)} \right)$$



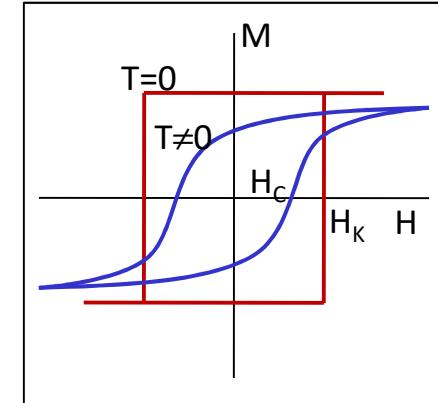
$$H_C(0) = 0.479 H_K$$



Temperature Dependent Magnetic Properties of Barium-Ferrite Thin-Film Recording Media

Yingjian Chen, *Member, IEEE*, and Mark H. Kryder, *Fellow, IEEE*

IEEE TRANSACTIONS ON MAGNETICS, VOL. 34, NO. 3, MAY 1998



$$H_c(T) \approx c H_K \left(1 - \left[\frac{kT}{KV} \ln(\tau_{\text{exp}} / \tau_0) \right]^n \right)$$

$$\nearrow c = 1$$

introduciendo

$$T_B = \frac{KV}{k \ln(\tau_{\text{exp}} / \tau_0)}$$

the easy axis orientation. In a system with uniaxially aligned easy axes, n is 1/2 [29], and in a system with random easy axis orientations, n is 2/3 [30]. The fitting parameters V_{sw}

- [29] M. P. Sharrock and J. T. McKinney, *IEEE Trans. Magn.*, vol. MAG-17, p. 3020, 1981.
- [30] R. H. Victora, "Predicted time dependence of the switching field for magnetic materials," *Phys. Rev. Lett.*, vol. 63, pp. 457–460, 1989.

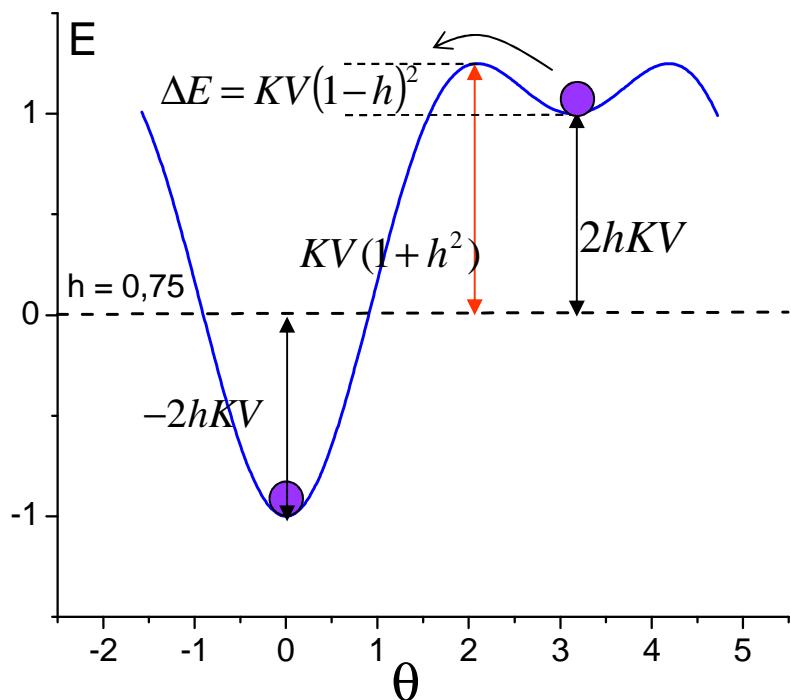
$$\searrow c = 0.48$$

$$H_c = c \frac{2K}{\mu_0 M_s} \left[1 - \left(\frac{T}{T_B} \right)^{1/2} \right]$$

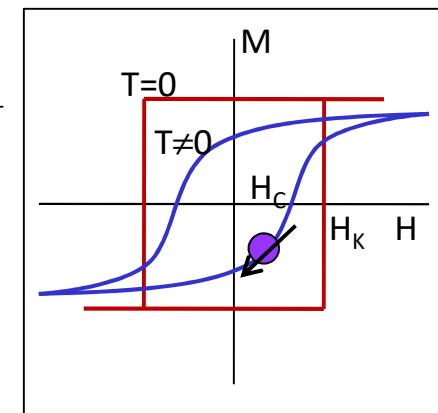
expresión de uso extendido

Dependencia del campo coercitivo con la temperatura 2

$$h = H / H_K = \frac{\mu_0 M_S H}{2K}$$



$$H_C = H_K = \frac{2K}{\mu_0 M_S}$$

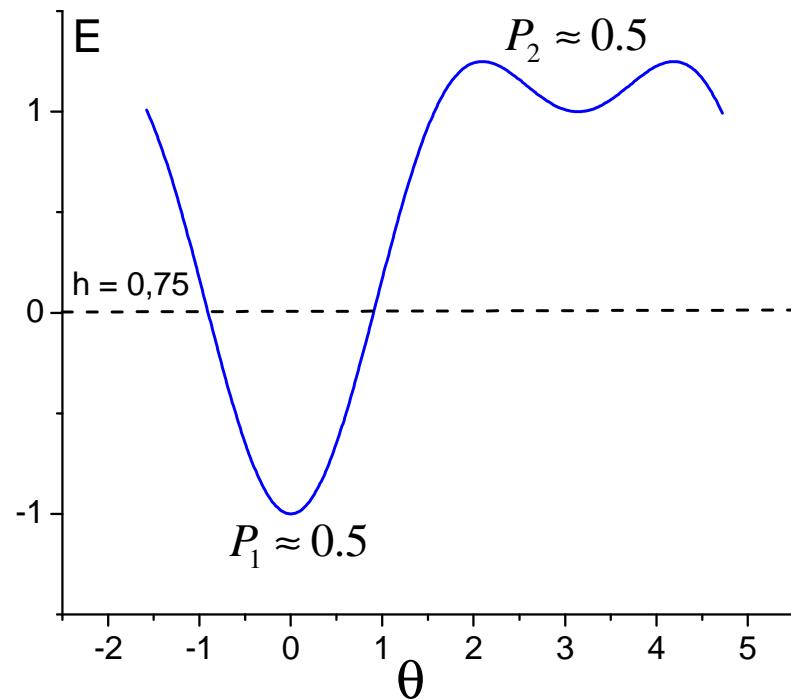


a $T \neq 0$ K la inversión de M se producirá cuando $\tau_{21} \approx \tau_{\text{exp}}$

$$\tau_{12} = \tau_0 e^{-\frac{KV(1+h)^2}{kT}} \quad f_{12} = v_0 e^{-\frac{KV(1+h)^2}{kT}}$$

$$\tau_{21} = \tau_0 e^{-\frac{KV(1-h)^2}{kT}} \quad f_{21} = v_0 e^{-\frac{KV(1-h)^2}{kT}}$$

Población de los estados orientacionales



$$P_1 + P_2 = 1$$

$$M \approx 0 \rightarrow P_1 \approx P_2 \approx 0.5$$

Evolución temporal
Por el principio del balance detallado

$$\frac{dP_1}{dt} = P_2 f_{21} - P_1 f_{12}$$

$$\frac{dP_1}{dt} \approx 0.5(f_{21} - f_{12})$$

$$M = M_s(P_1 - P_2) = M_s(2P_1 - 1)$$

$$\frac{dM}{dt} = 2M_s \frac{dP_1}{dt} \approx M_s(f_{21} - f_{12})$$

$$\frac{1}{\nu_0 M_s} \frac{dM}{dt} \approx e^{-\frac{KV(1-h)^2}{kT}} - e^{-\frac{KV(1+h)^2}{kT}}$$

$$\frac{1}{\nu_0 M_s} \frac{dM}{dt} \approx e^{-\frac{KV(1-h)^2}{kT}} - e^{-\frac{KV(1+h)^2}{kT}} \approx e^{-\frac{KV(1-h)^2}{kT}}$$

$$\frac{1}{\nu_0 M_s} \frac{dM}{dt} \approx e^{-\frac{KV(1-h)^2}{kT}} - e^{-\frac{KV(1+h)^2}{kT}} \approx e^{-\frac{KV(1-h)^2}{kT}}$$

$$\frac{dM}{dt} = \frac{dM}{dH} \frac{dH}{dt}$$

cuando $H \approx H_c \rightarrow \frac{dM}{dH} = \chi \approx cte$

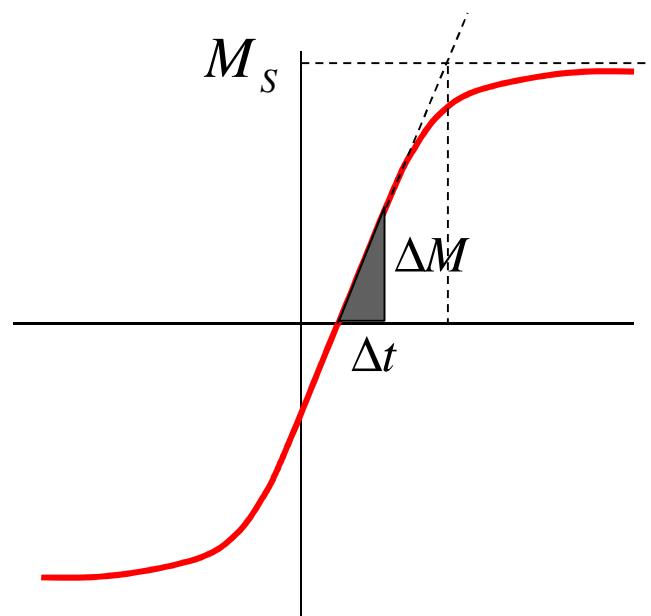
$$\frac{1}{\nu_0 M_s} \chi \frac{dH}{dt} \Big|_{H_c} \approx e^{-\frac{KV(1-h_c)^2}{kT}}$$

$$H_c \approx H_K \left\{ 1 - \sqrt{\frac{kT}{KV} \ln \left[\frac{M_s}{\chi(dH/dt)_{H_c}} \frac{1}{\tau_0} \right]} \right\}$$

$\tau_0 = 1/c_0$

escribiendo $\chi \approx \Delta M / \Delta H$, $dH / dt \approx \Delta H / \Delta t$

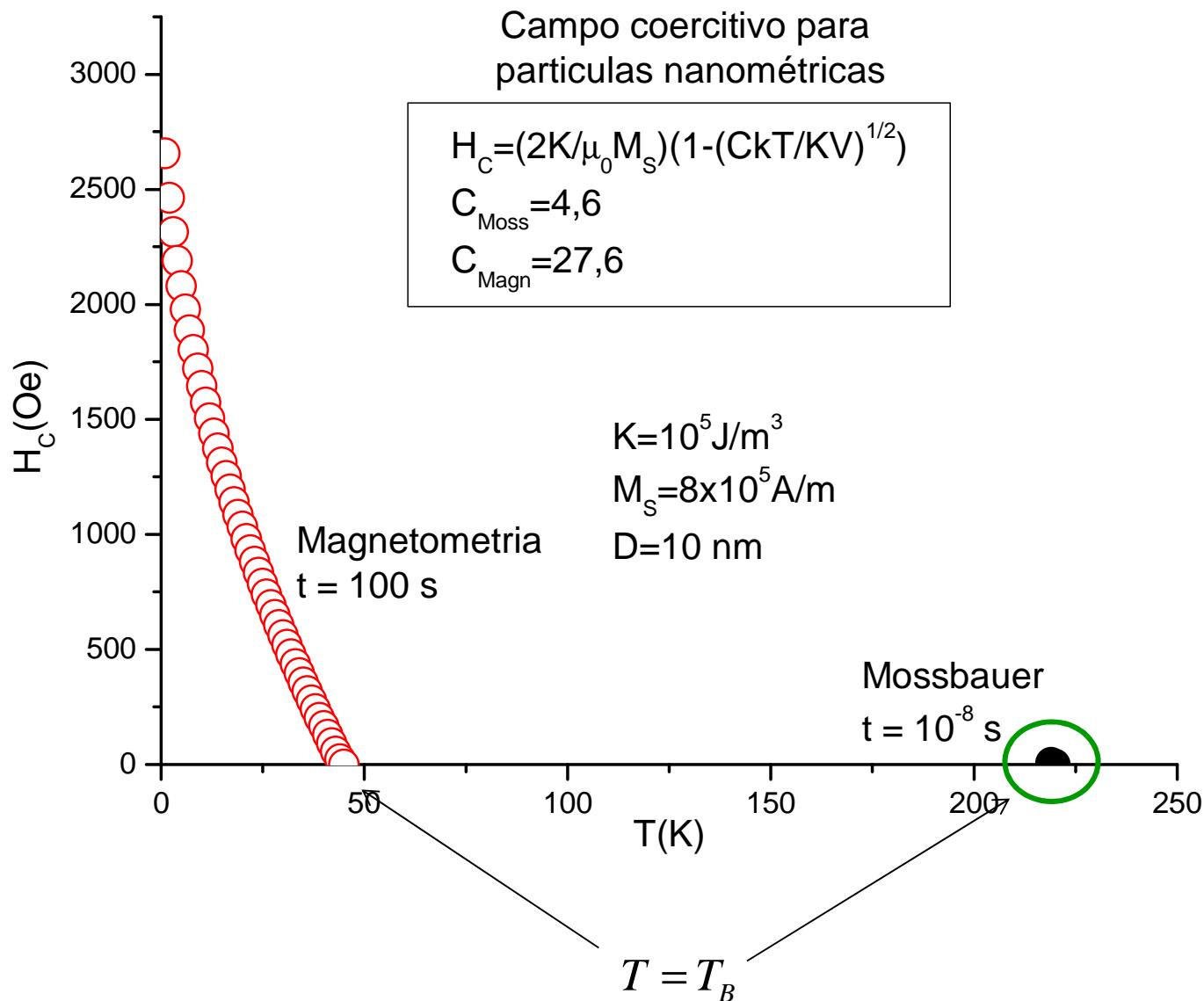
$$H_C \approx H_K \left\{ 1 - \sqrt{\frac{kT}{KV} \ln \left[\frac{(M_S / \Delta M) \Delta t}{\tau_0} \right]} \right\}$$



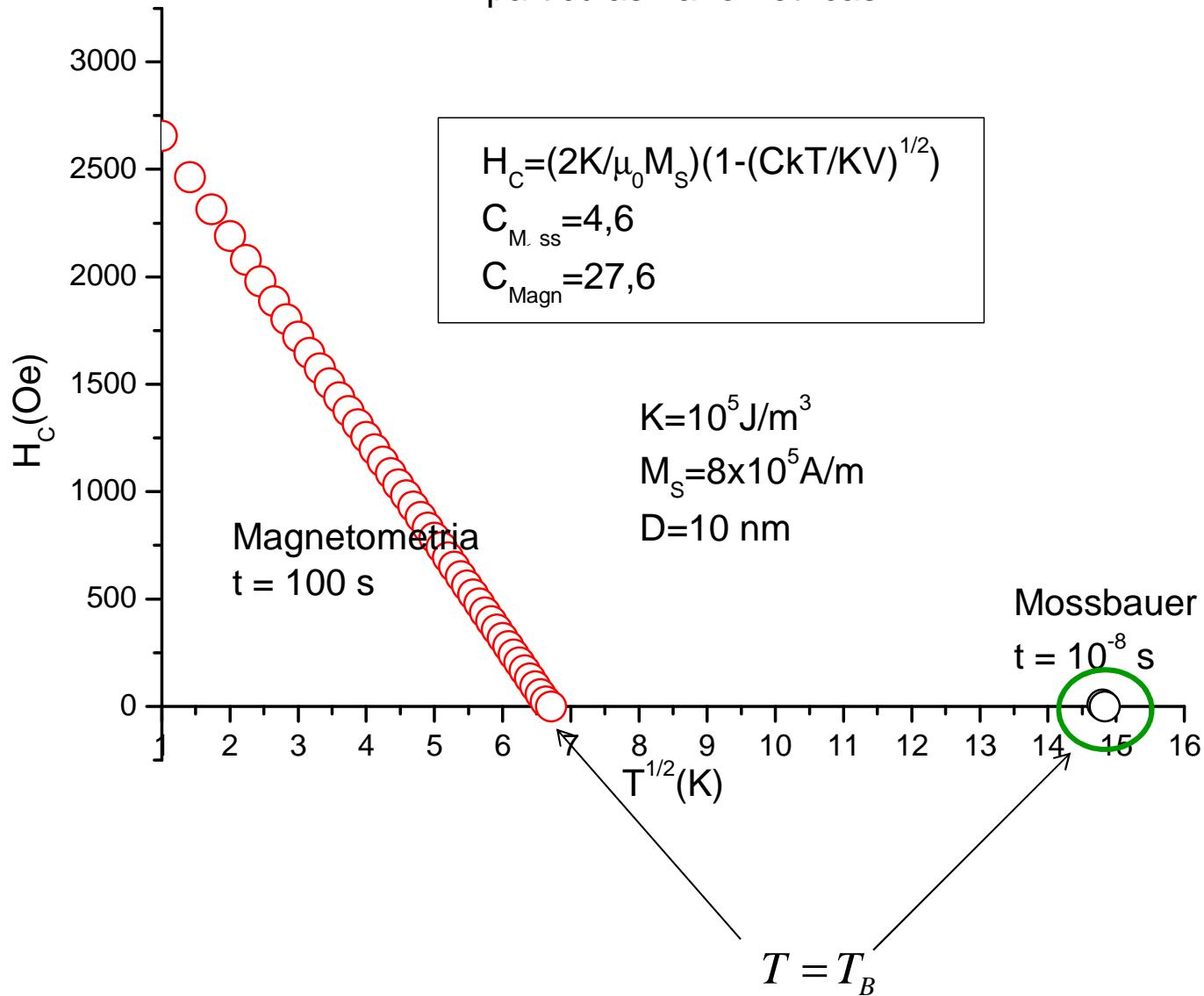
Llamando $n = M_S / \Delta M$ $\tau_{\text{exp}} = n \Delta t$

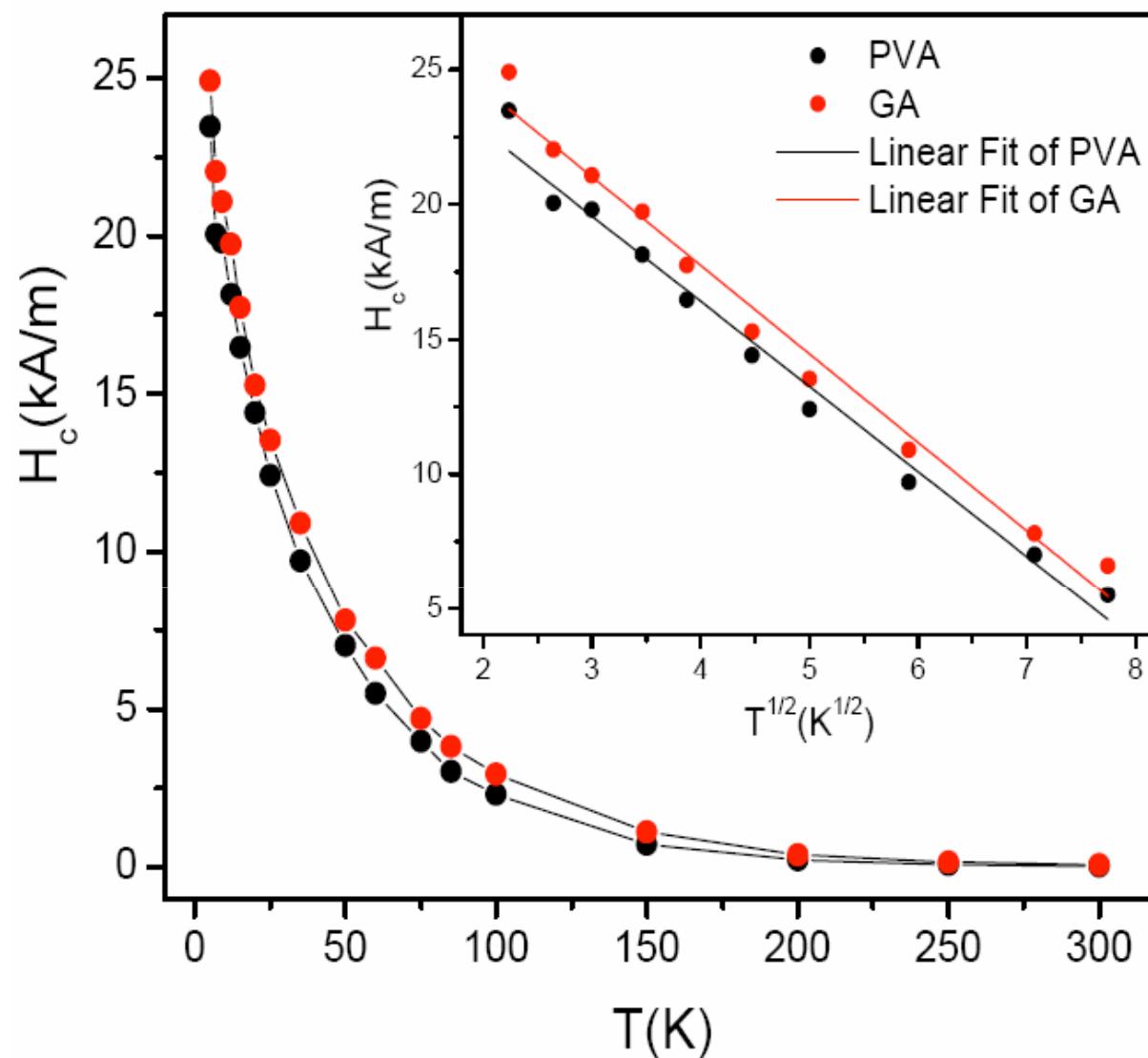
$$H_C \approx H_K \left\{ 1 - \sqrt{\frac{kT}{KV} \ln \left(\frac{\tau_{\text{exp}}}{\tau_0} \right)} \right\}$$

Donde τ_{exp} sería el tiempo aproximado requerido para alcanzar la saturación desde $M = 0$



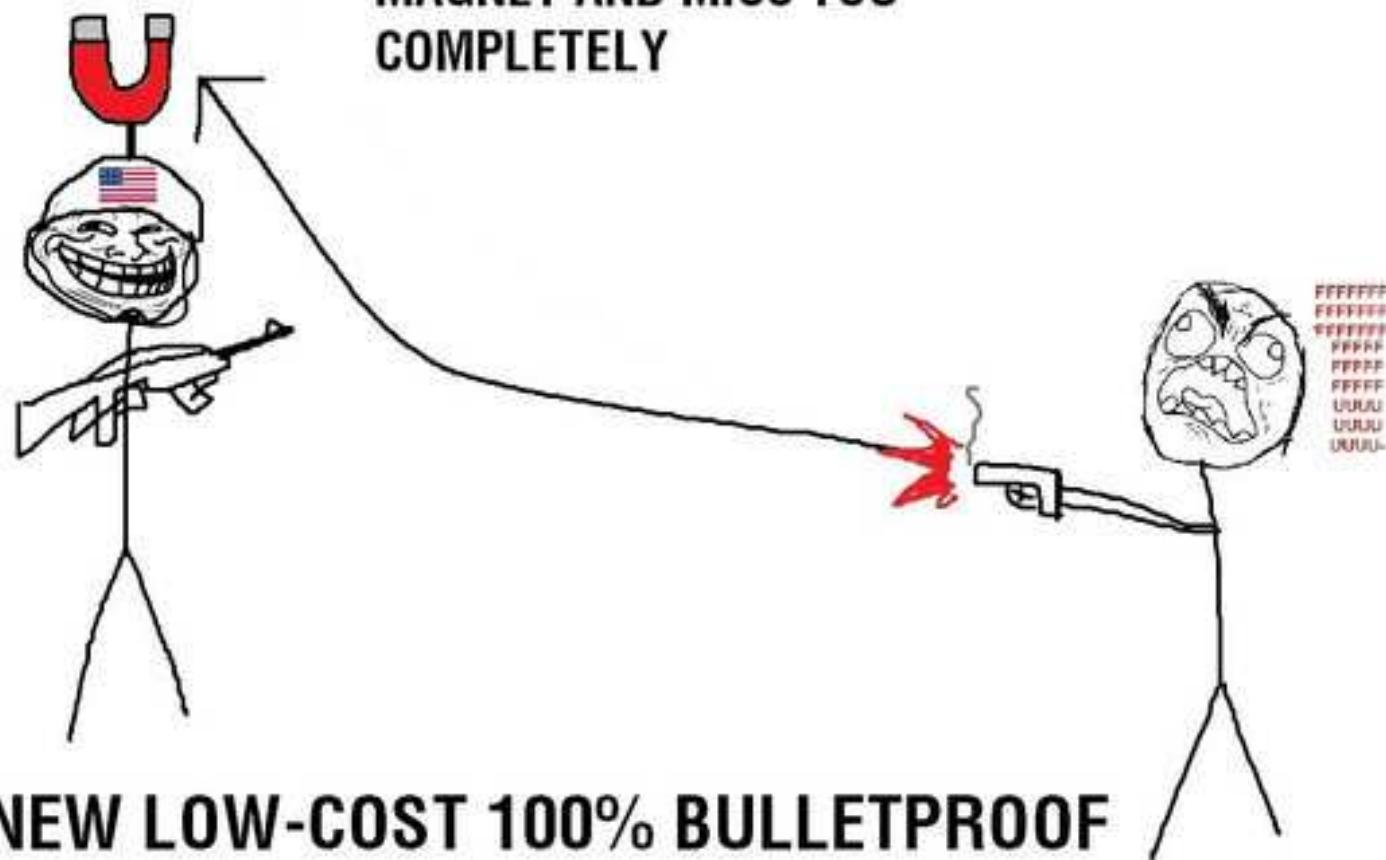
Campo coercitivo para partículas nanométricas





Ferrogel de NP de magnetita (8 nm) en hidrogel de PVA, Mendoza
Zélis et al, enviado

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